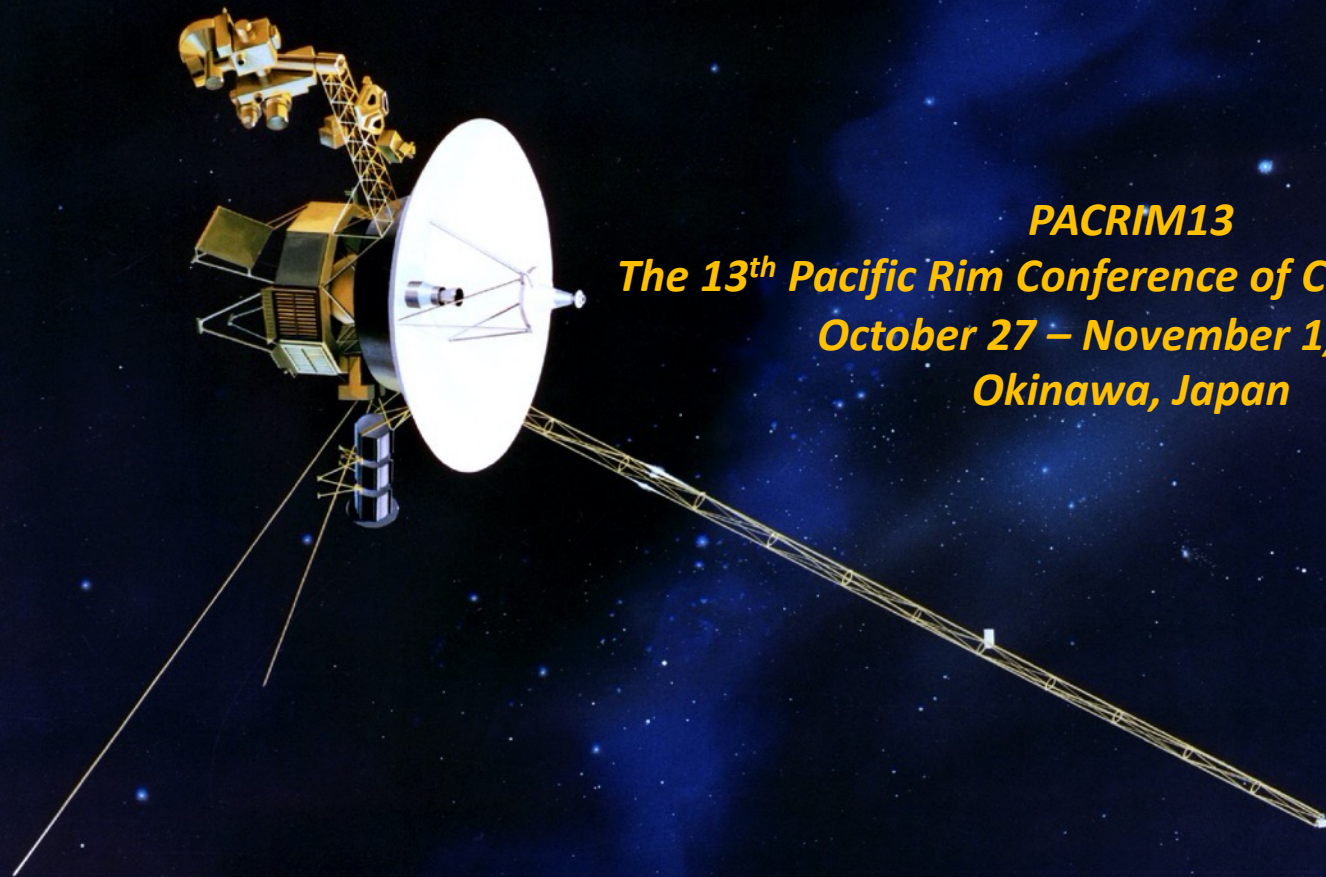




Life Performance Prediction Approach for the Potential eMMRTG

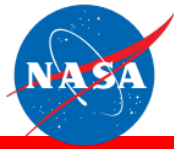


PACRIM13
The 13th Pacific Rim Conference of Ceramic Societies
October 27 – November 1, 2019
Okinawa, Japan

T. Caillat¹, I. Chi¹, J. Paik¹, S. Pinkowski¹, C. Matthes¹, and M. Hoffmann²

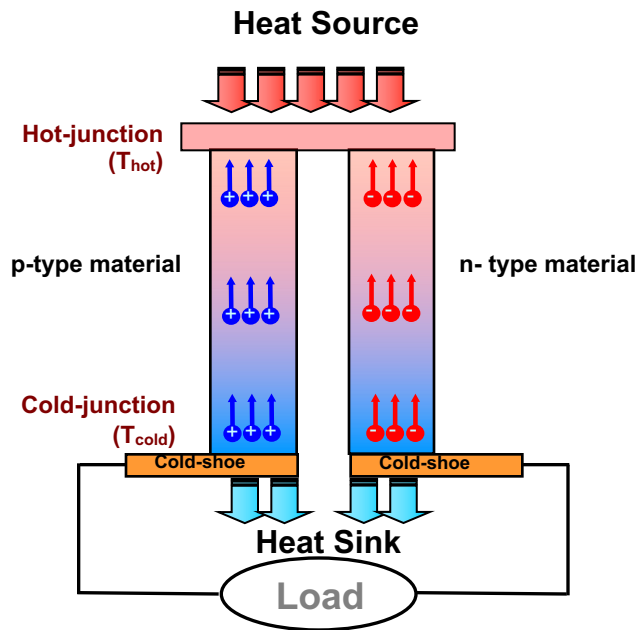
**¹Jet Propulsion Laboratory/California Institute of Technology
Pasadena, CA, USA**

**²NASA Glenn Research Center
Cleveland, OH, USA**



Thermoelectric Power Generation

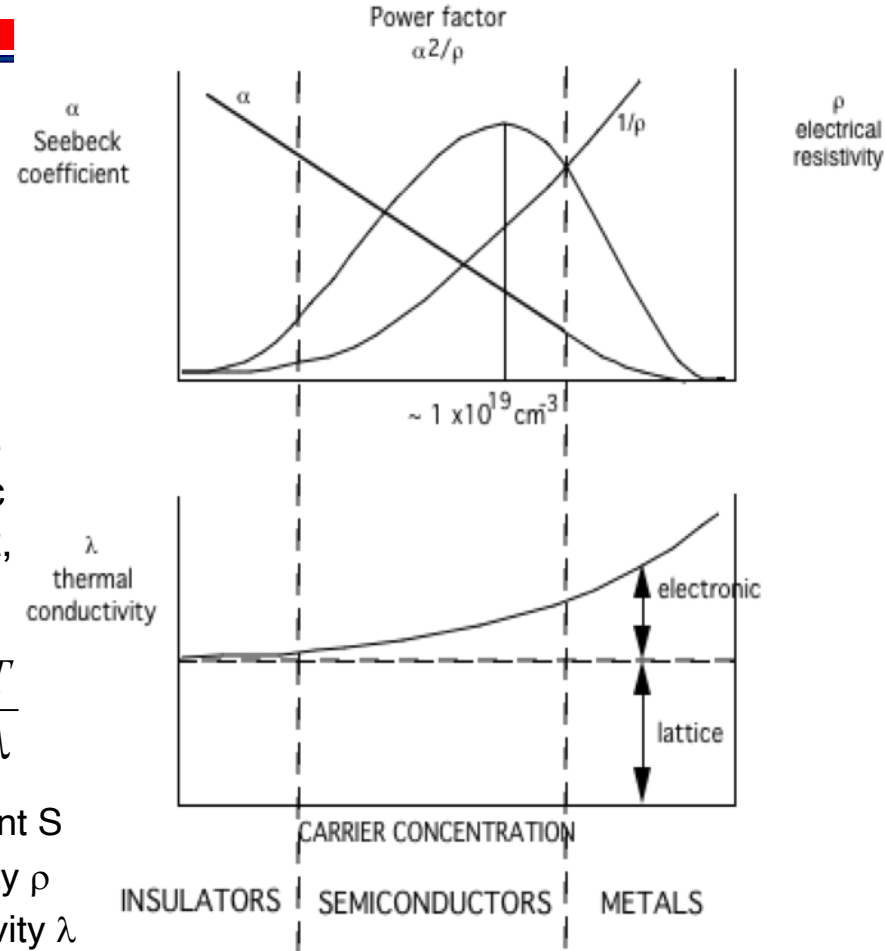
Thermoelectric effects are defined by a coupling between the electrical and thermal currents induced by an electric field and a temperature gradient



Dimensionless Thermoelectric Figure of Merit, ZT

$$ZT = \frac{\sigma S^2 T}{\lambda} = \frac{S^2 T}{\rho \lambda}$$

- Seebeck coefficient S
- Electrical resistivity ρ
- Thermal conductivity λ



Thermoelectric Couple

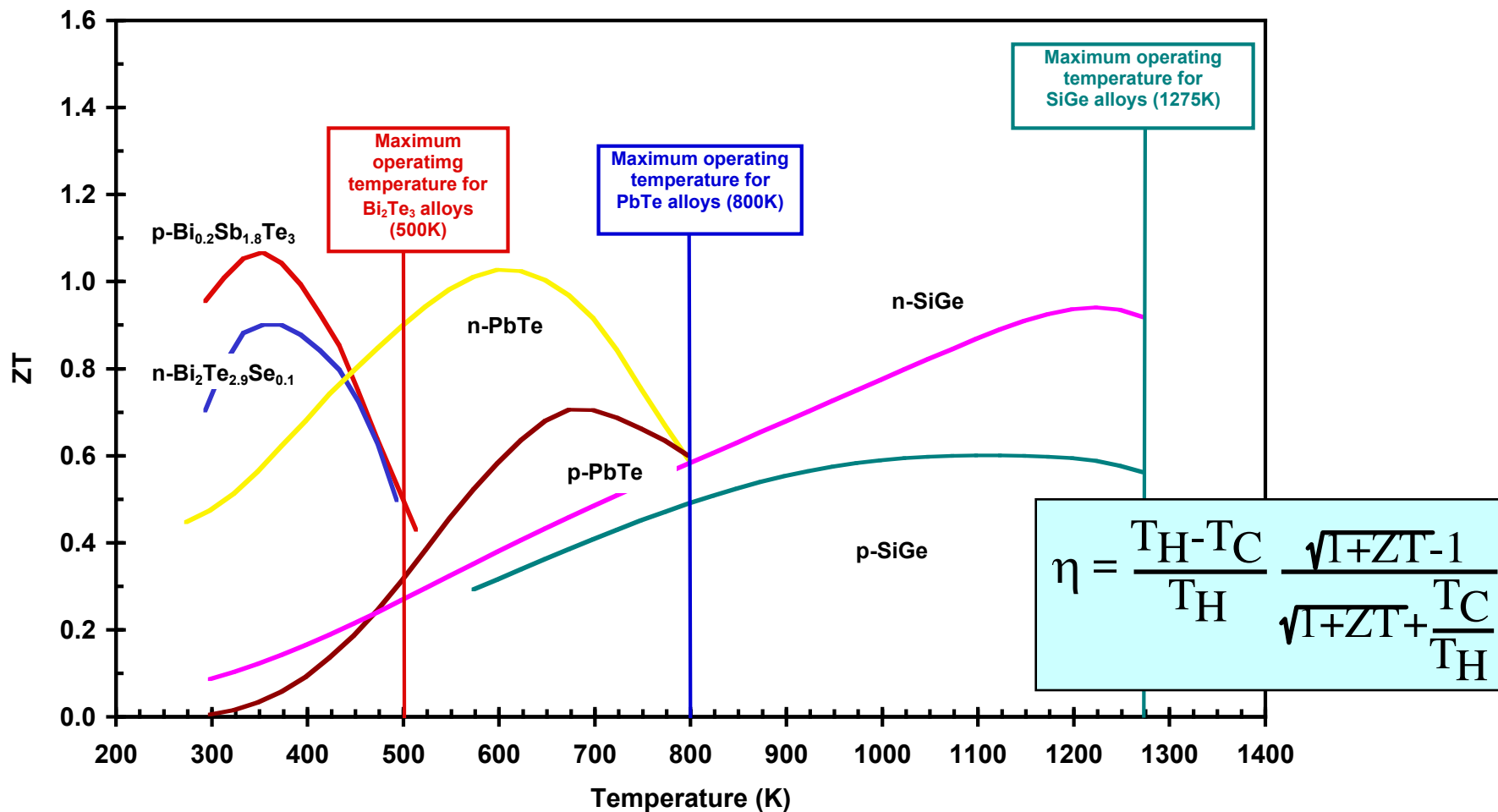
Conversion efficiency is function of ZT and ΔT

Conversion Efficiency

$$\eta_{\max} = \frac{\text{Carnot}}{\text{TE Materials}} = \frac{T_{\text{hot}} - T_{\text{cold}}}{T_{\text{hot}}} \frac{\sqrt{1 + ZT} - 1}{\sqrt{1 + ZT} + \frac{T_{\text{cold}}}{T_{\text{hot}}}}$$



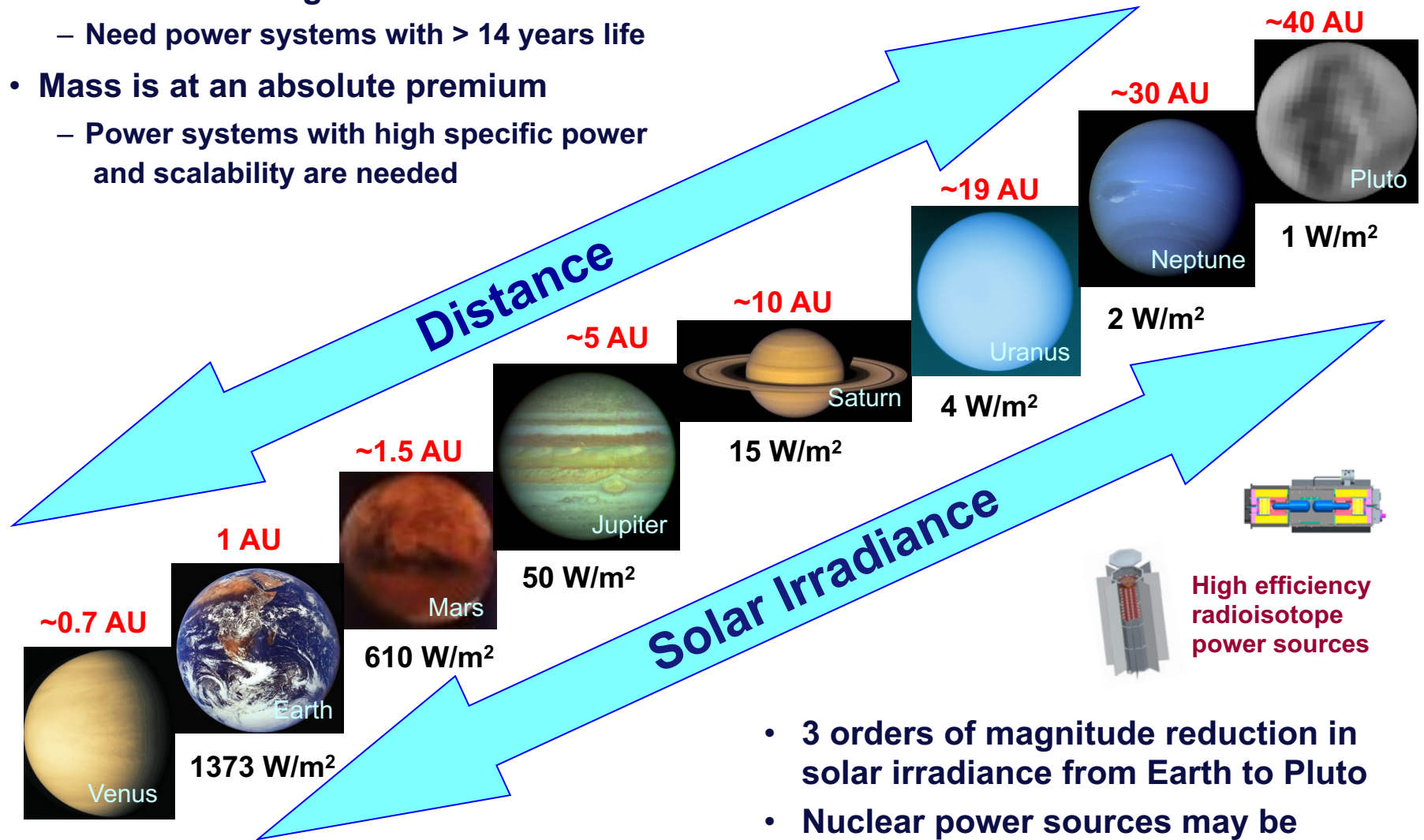
State-of-Practice High-Temperature Thermoelectric Materials





Space Power Technology

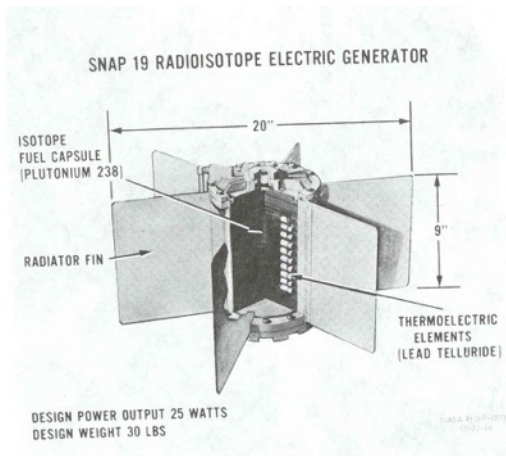
- Missions are long
 - Need power systems with > 14 years life
- Mass is at an absolute premium
 - Power systems with high specific power and scalability are needed



- 3 orders of magnitude reduction in solar irradiance from Earth to Pluto
- Nuclear power sources may be needed for some missions



Flight Demonstrated Radioisotope Thermoelectric Generators (3 Most Recently Flown Designs)



SNAP-19 (PbTe/TAGS RTG)
(1960-70' s)

40.3 Watts (BOM)
6.2 % system efficiency
3 We/kg

PbTe Thermoelectrics
 $T_H = 525C$, $T_C = 210C$

Nimbus B-1/III, Pioneer 10/11,
Viking 1/2

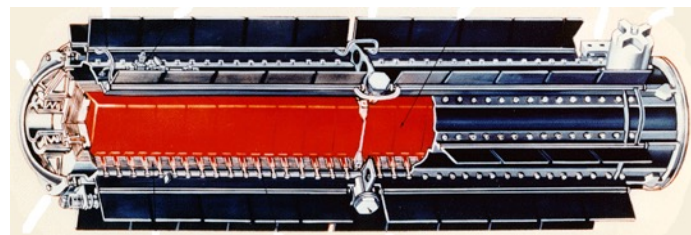


SiGe MHW RTG
(1970' s)

158 We (BOM)
6.6 % system efficiency
4.2 We/kg

SiGe Thermoelectrics
 $T_H = 1000C$, $T_C = 300C$

LES 8/9, Voyager 1/2



SiGe GPHS RTG
(1980-2006)

285 We (BOM)
6.8% system efficiency
5.1 We/kg

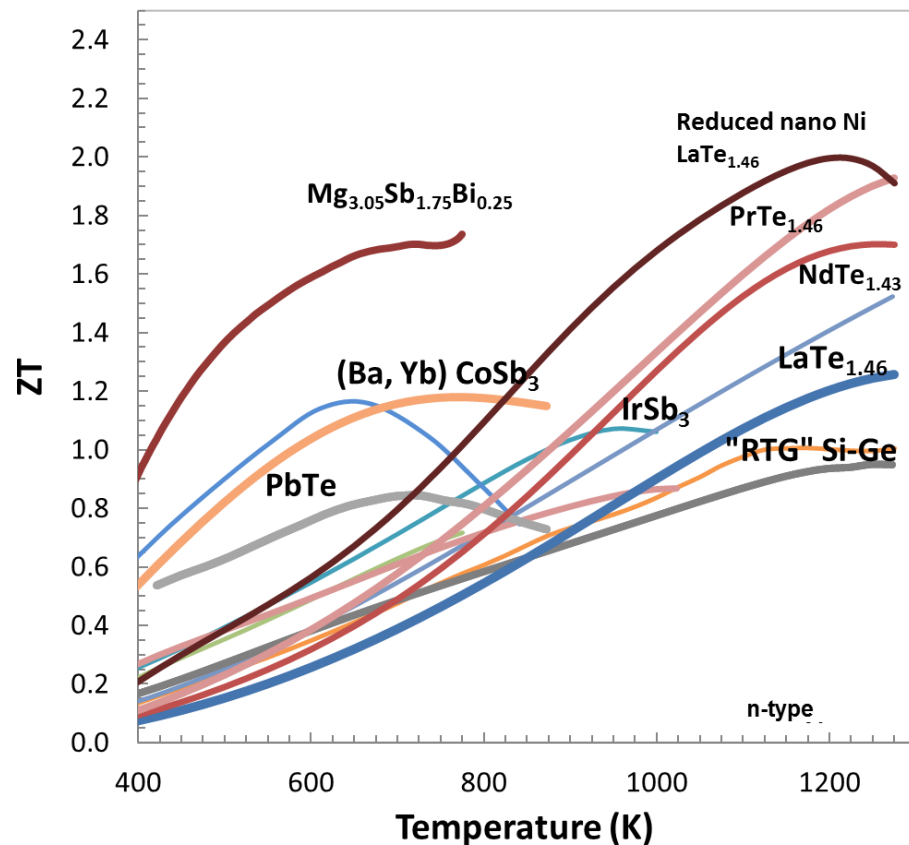
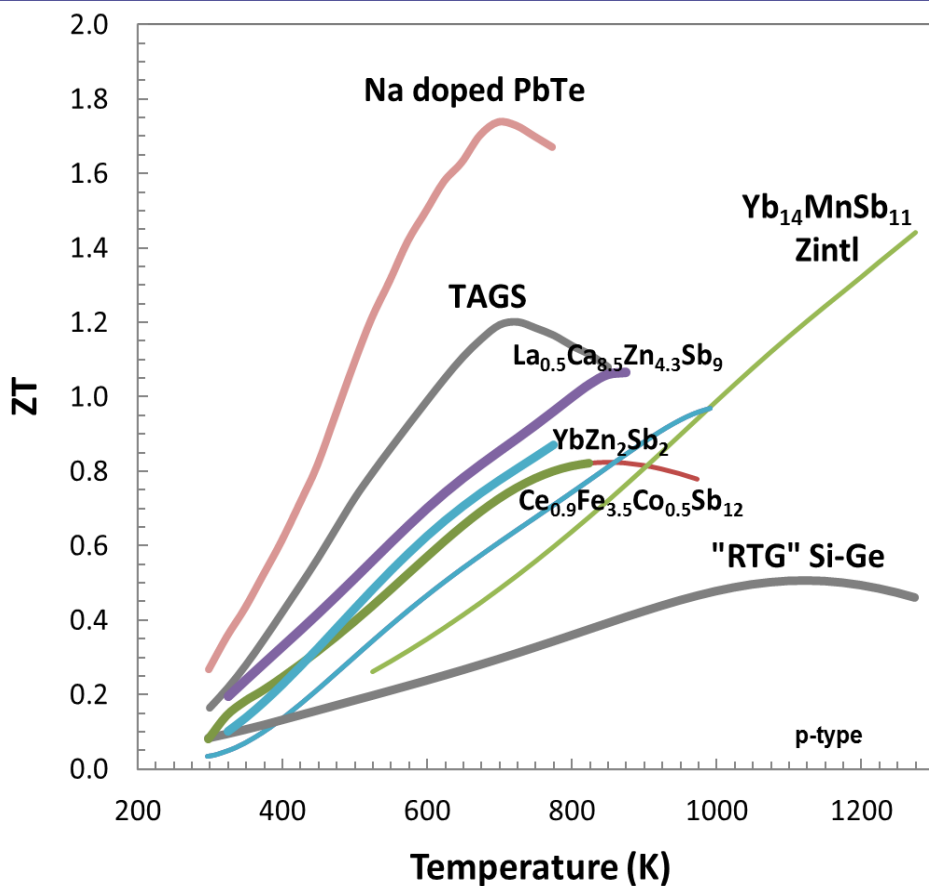
SiGe Thermoelectrics
 $T_H = 1000C$, $T_C = 300C$

Galileo, Ulysses, Cassini
& New Horizons

Past US Radioisotope Power Systems have used either PbTe or SiGe alloys thermoelectric materials



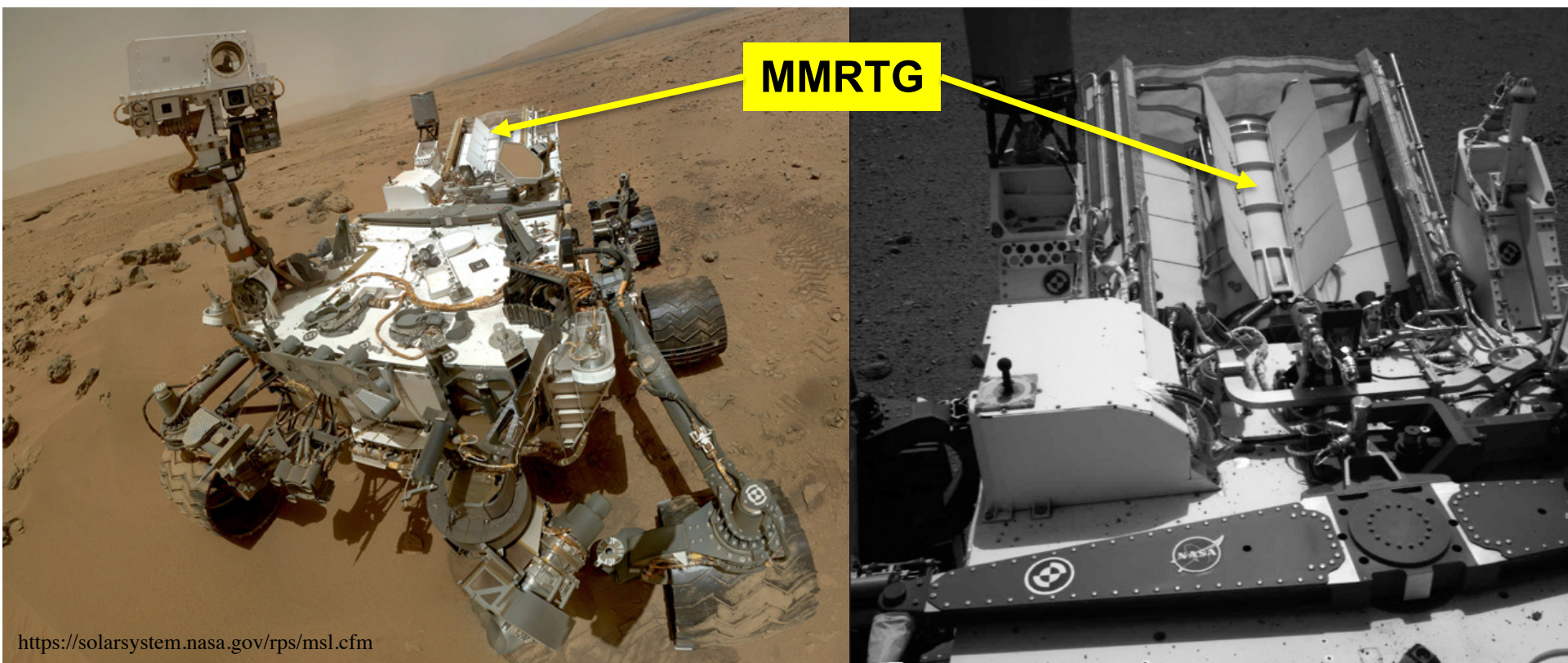
JPL Advanced TE Materials



- Best combination of TE materials predicted to result in $\sim 18\%$ couple-level efficiency
- Some advanced TE materials under development for device integration



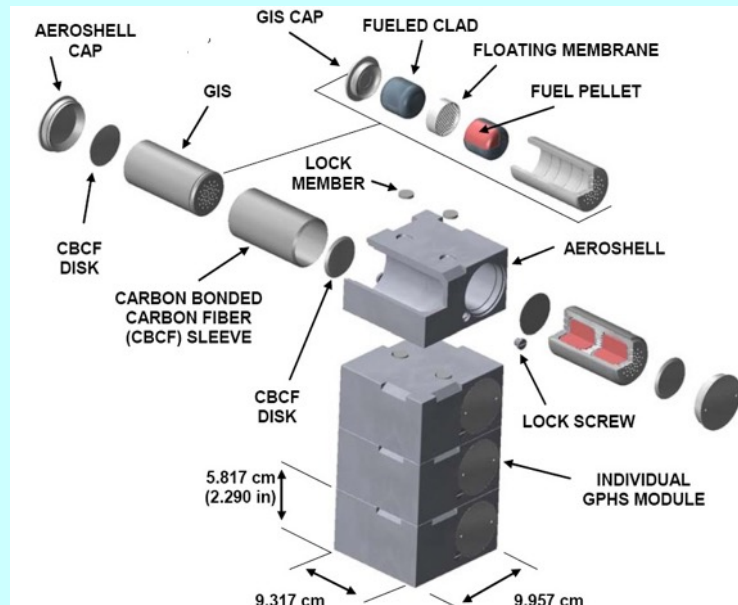
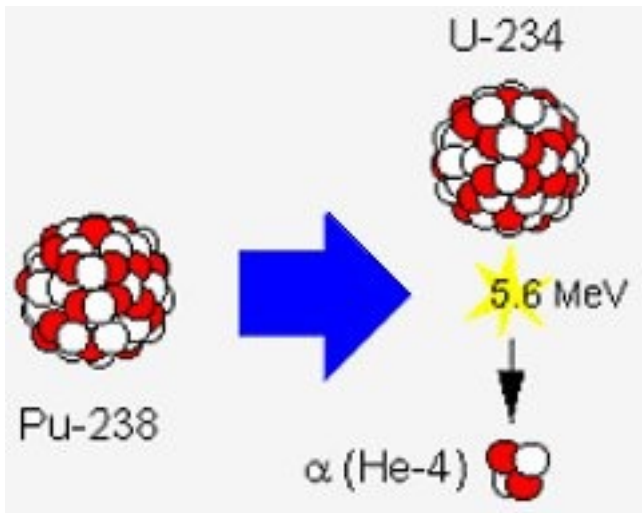
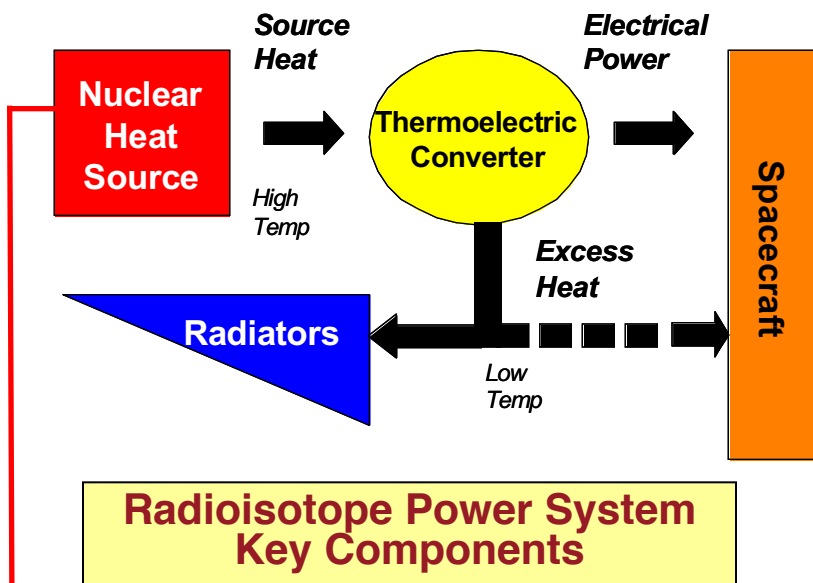
MSL Curiosity Rover Powered by the Multi-Mission Radioisotope Thermoelectric Generator (MMRTG)



MMRTG has successfully and reliably provided power and thermal energy to the Curiosity rover since August 2012. It will fly again on Mars 2020.



Radioisotope Thermoelectric Generator Key Components



https://en.wikipedia.org/wiki/General-purpose_heat_source

• General Purpose Heat Source (GPHS)

- Uses ^{238}Pu
 - Decay
 - α emitter
 - 87.7 years half-life
- 440 g ^{238}Pu per GPHS
- 250 thermal Watts/GPHS
- Heat flux ~ a few W/cm²
- $T_H > 1000\text{C}$



Many RT_4Pn_{12} compounds exist such as

$LaFe_4As_{12}$

Derived from $CoAs_3$ skutterudite prototype:

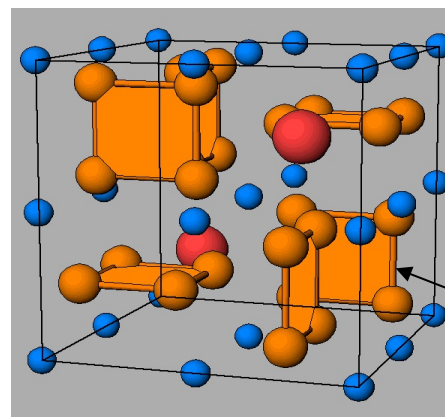
- By filling the empty octants present in the unit cell

Most have a metallic behavior

- Trivalent rare earth (La^{3+}) and divalent transition metal (Fe^{2+})
- Valence electron count $(1 \times 3) + (4 \times 8) + (12 \times 3) = 71$
- Count of 72 needed to conserve a semiconducting behavior

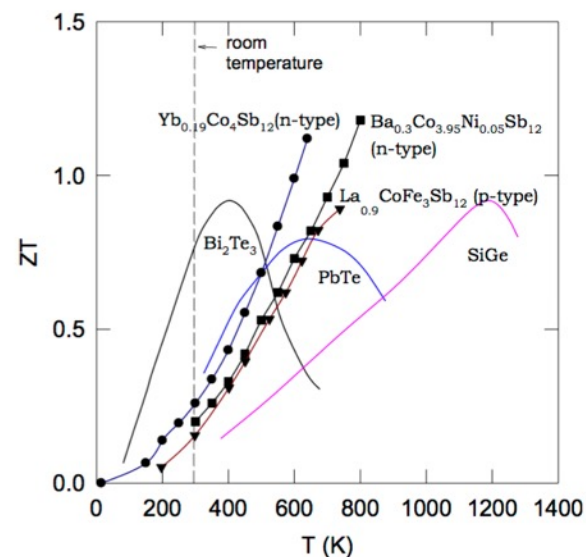
Expected reduction in lattice thermal conductivity

- “Rattlers”
 - Conduction in valence band dominated by pnictogen rings ; potentially, no significant impact on carrier mobility
- ⇒ Phonon Glass Electron Crystal (PGEC) concept (G. Slack): decoupling of electrical and thermal transport i.e. conduct electricity like a perfect crystal with a glass-like thermal conductivity



Skutterudite crystal structure

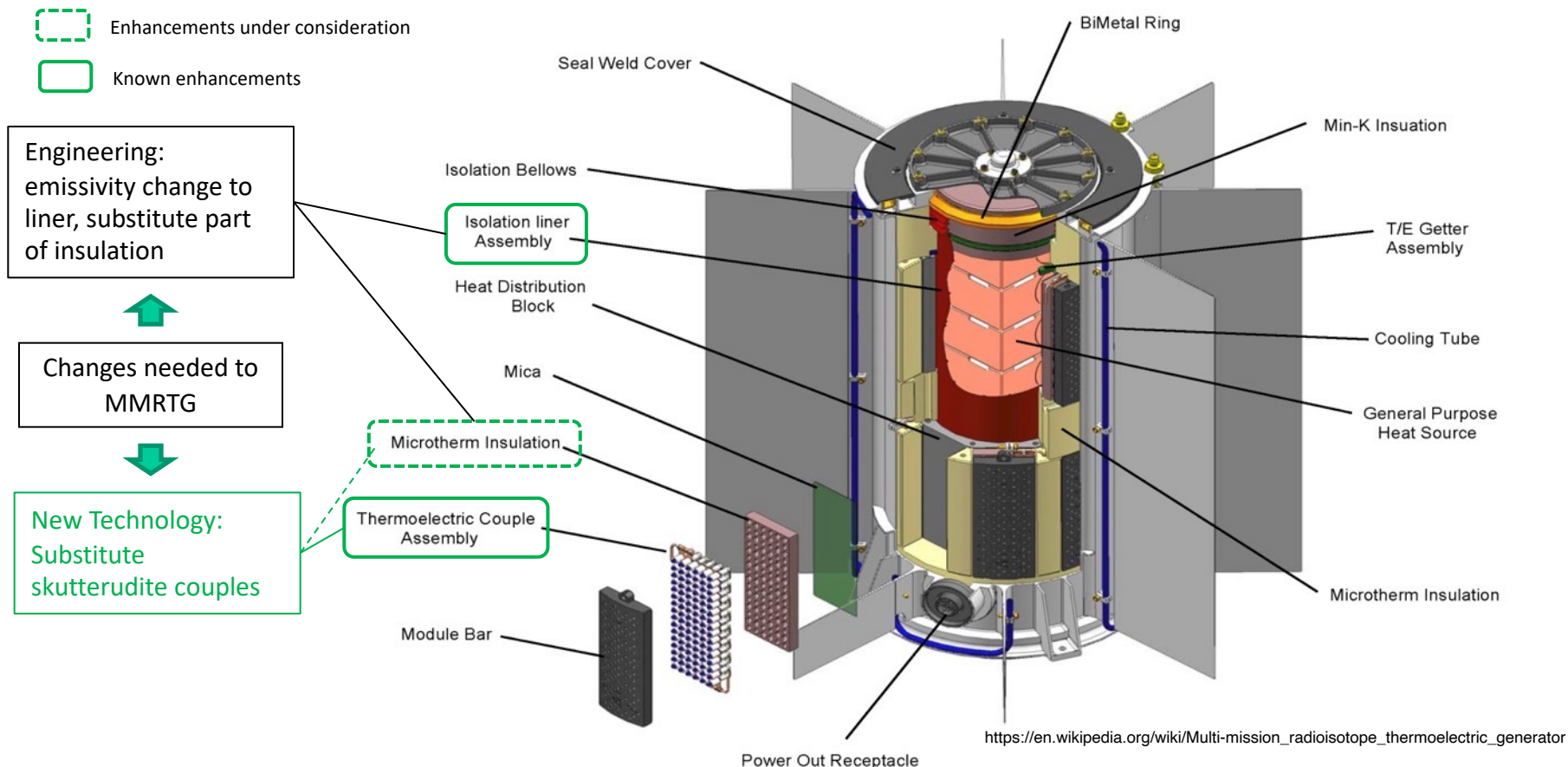
Pnictogen rings



Skutterudites have excellent thermoelectric properties with $ZT > 1$



What is being enhanced in the Proposed eMMRTG?



Retrofitting the MMRTG with new skutterudite thermoelectric couples

- Skutterudite couples fit within the space available (no change in number of couples, 768)
- Simple emissivity change to heat source liner will enable use of MMRTG end insulation system
- Volume, mass, and external interfaces remain unchanged
- Multi-mission capability preserved

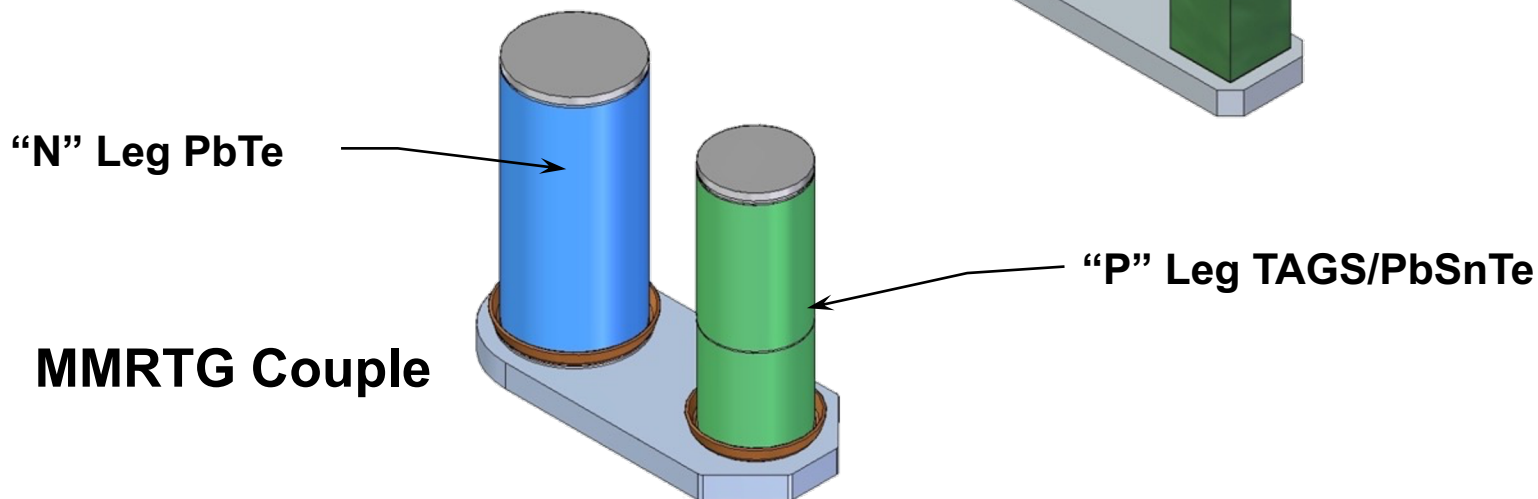
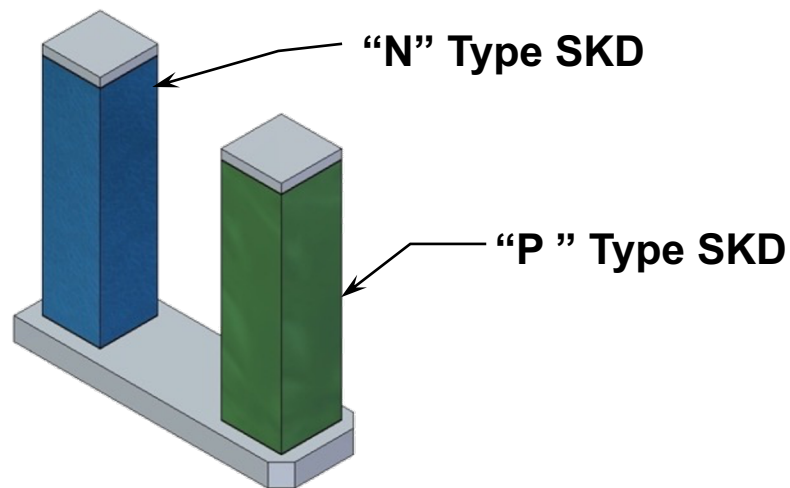


T/E Couple Assembly Comparison

“Drop-in Replacement” Couple

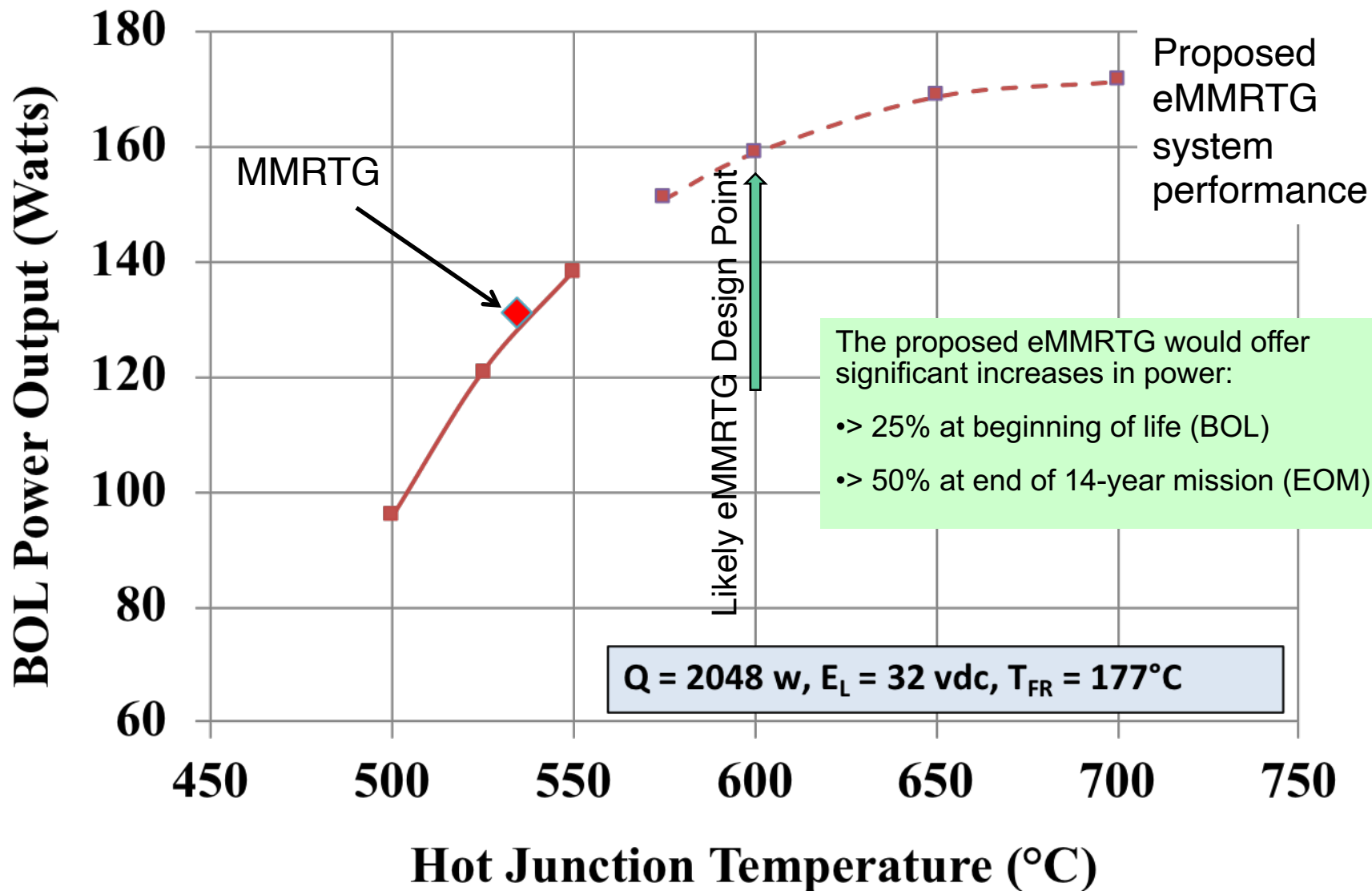
- Better high temperature capability
- Non-segmented
- Equivalent or better mechanical properties
- Smaller element cross section
 - *Required to increase hot side temperature*

Proposed eMMRTG Couple



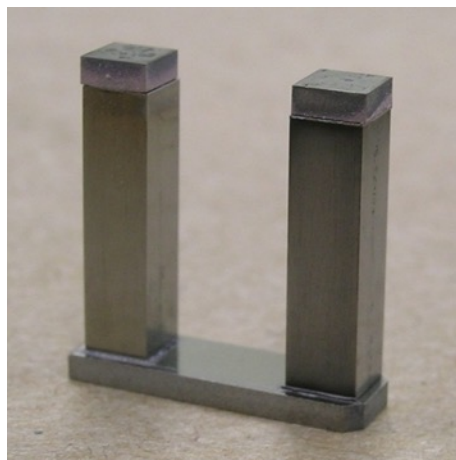


eMMRTG– Power vs. $T_{\text{hot-junction}}$

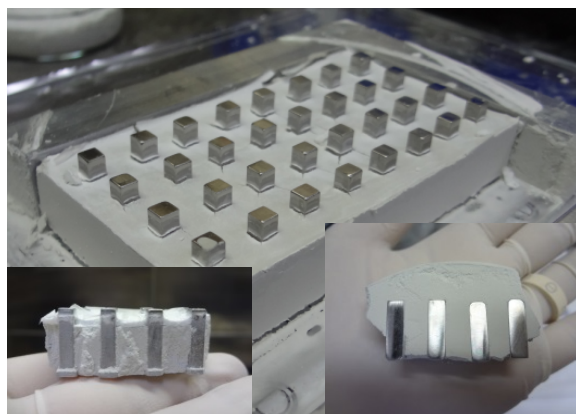




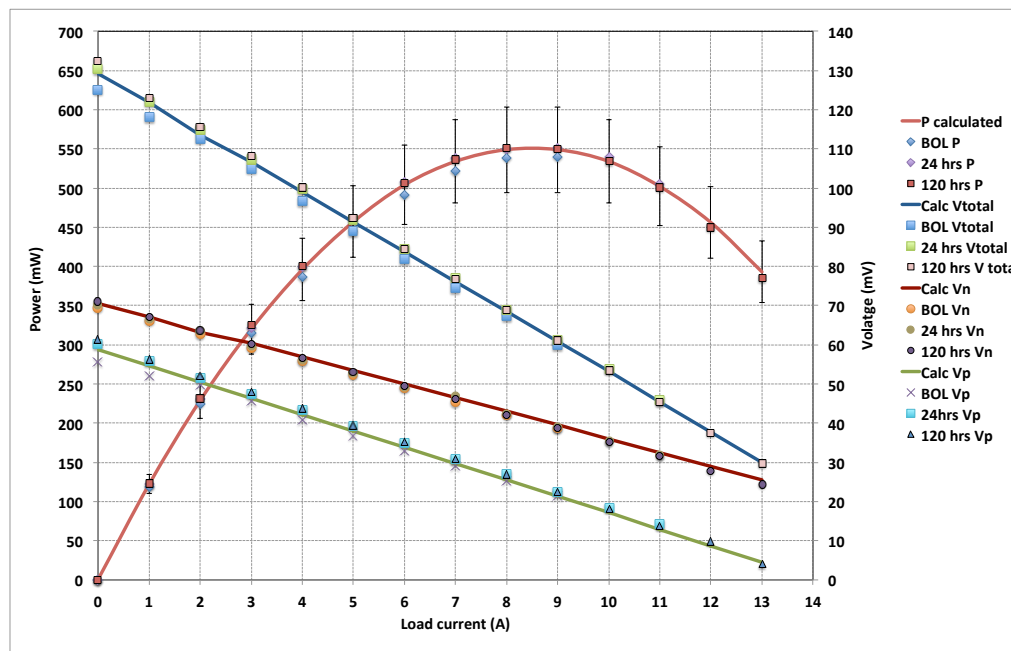
Couple Fabrication, Encapsulation, and Performance



1st iteration SKD couple



Critical Point Dried Aerogel Processed into a 4 x 8 Array of Couples

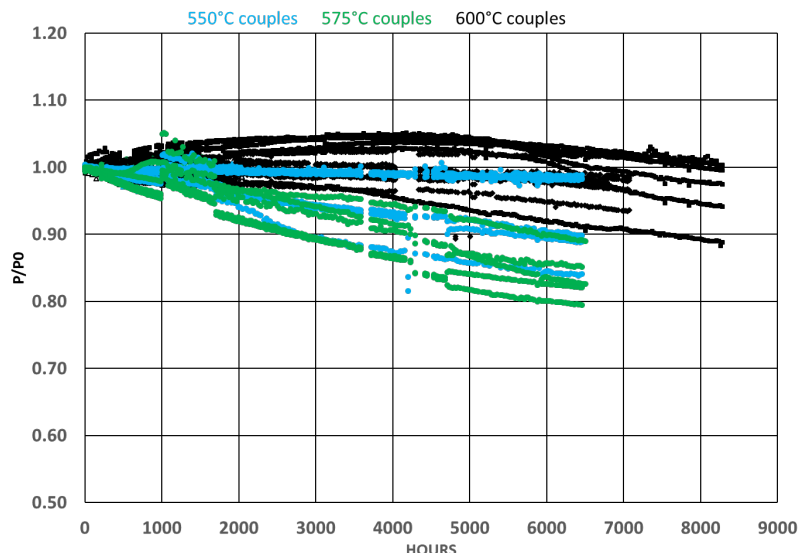


Couple ID	T_{Hot}	$T_{Cold-AVG}$	V_{OC}	Power at match-load			
				V_{load} (mV)	I (A)	P (mW)	Adj. P (mW)
SKD-64-1	601.6	199.9	133.6	66.55	3.57	237.7	234.0
SKD-64-2	601.2	199.9	130.8	65.07	3.49	227.0	235.1
SKD-64-3	601.1	199.9	134.2	66.66	3.60	240.0	234.3
SKD-64-4	601.3	199.9	133.2	66.37	3.60	239.0	239.0

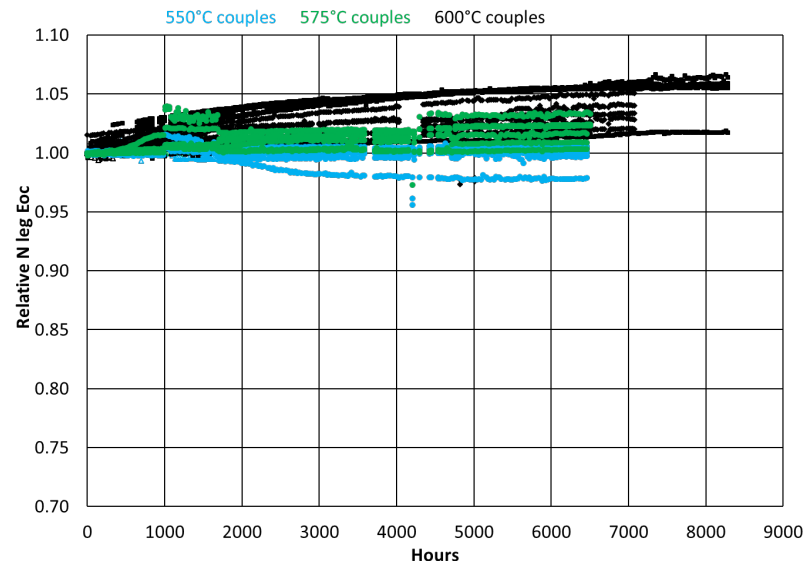


MMLT Couple Testing: n-legs 550-600

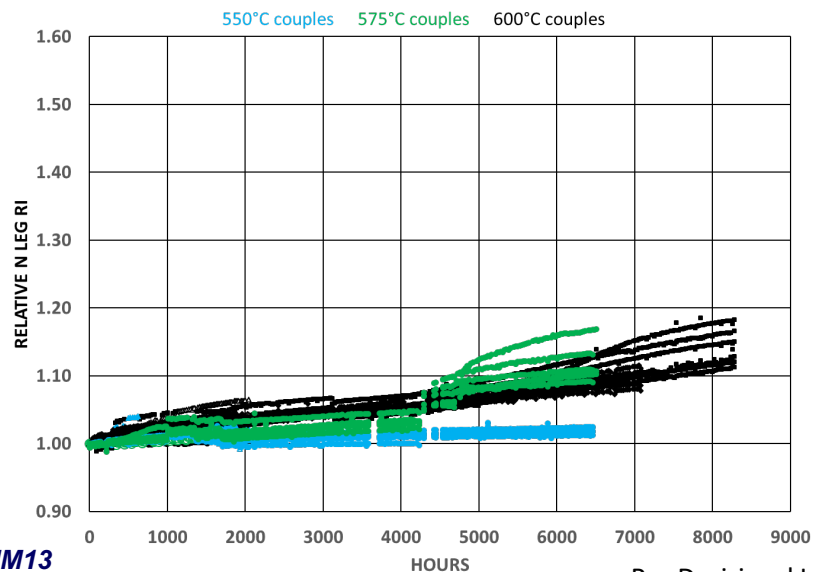
MMLT COUPLE TESTING - N LEG RELATIVE PEAK POWER



MMLT Couple Testing - N leg Open circuit voltage



MMLT COUPLE TESTING - N LEG INTERNAL RESISTANCE

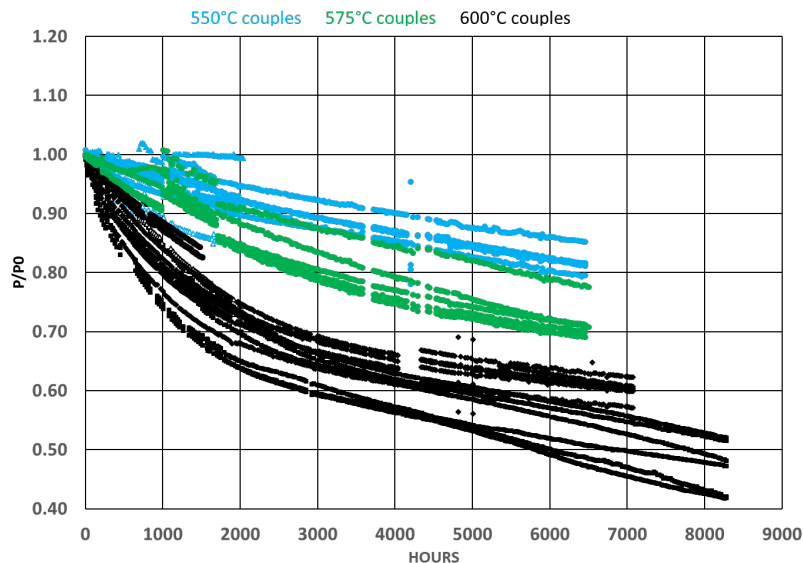


- N-legs show stable performance
- 600C actually shows slight rise in power
- Slight rise in internal resistance is compensated by rise in open circuit voltage
- Nominal Th_j operating temperature is about 550C

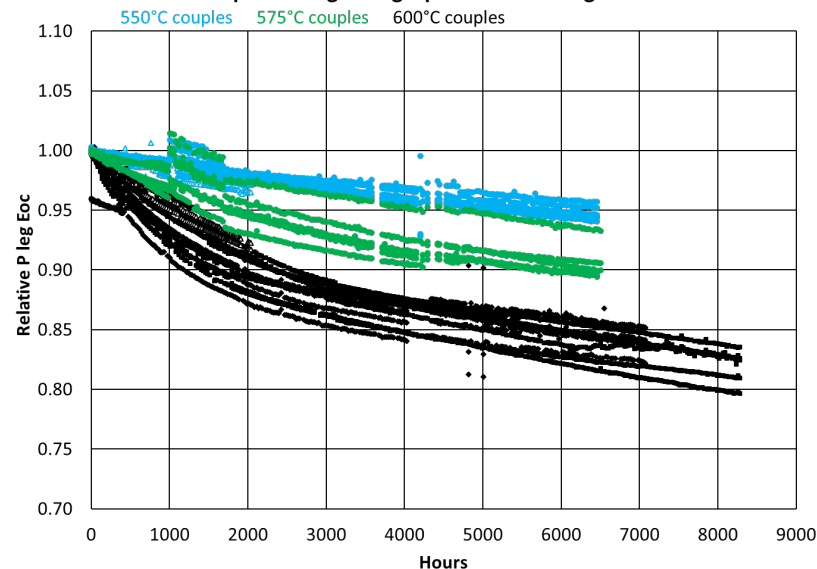


MMLT Couple Testing: P-legs 550-600

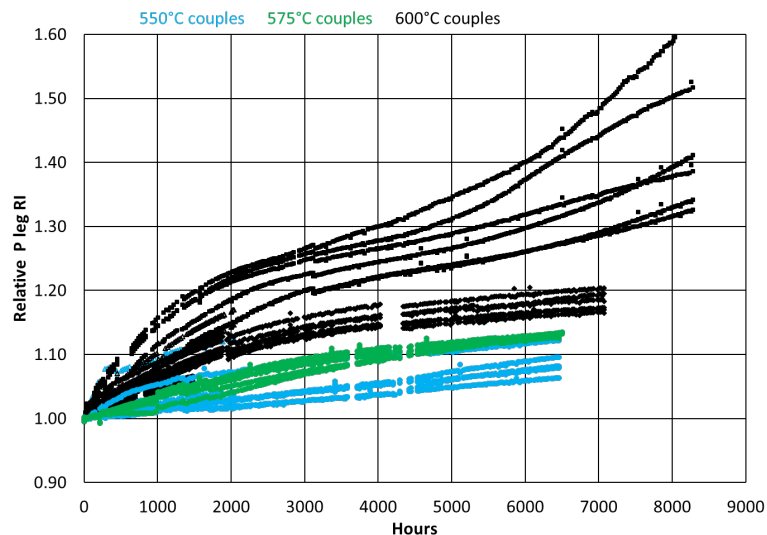
MMLT COUPLE TESTING - P LEG RELATIVE PEAK POWER



MMLT Couple Testing - P leg Open circuit voltage



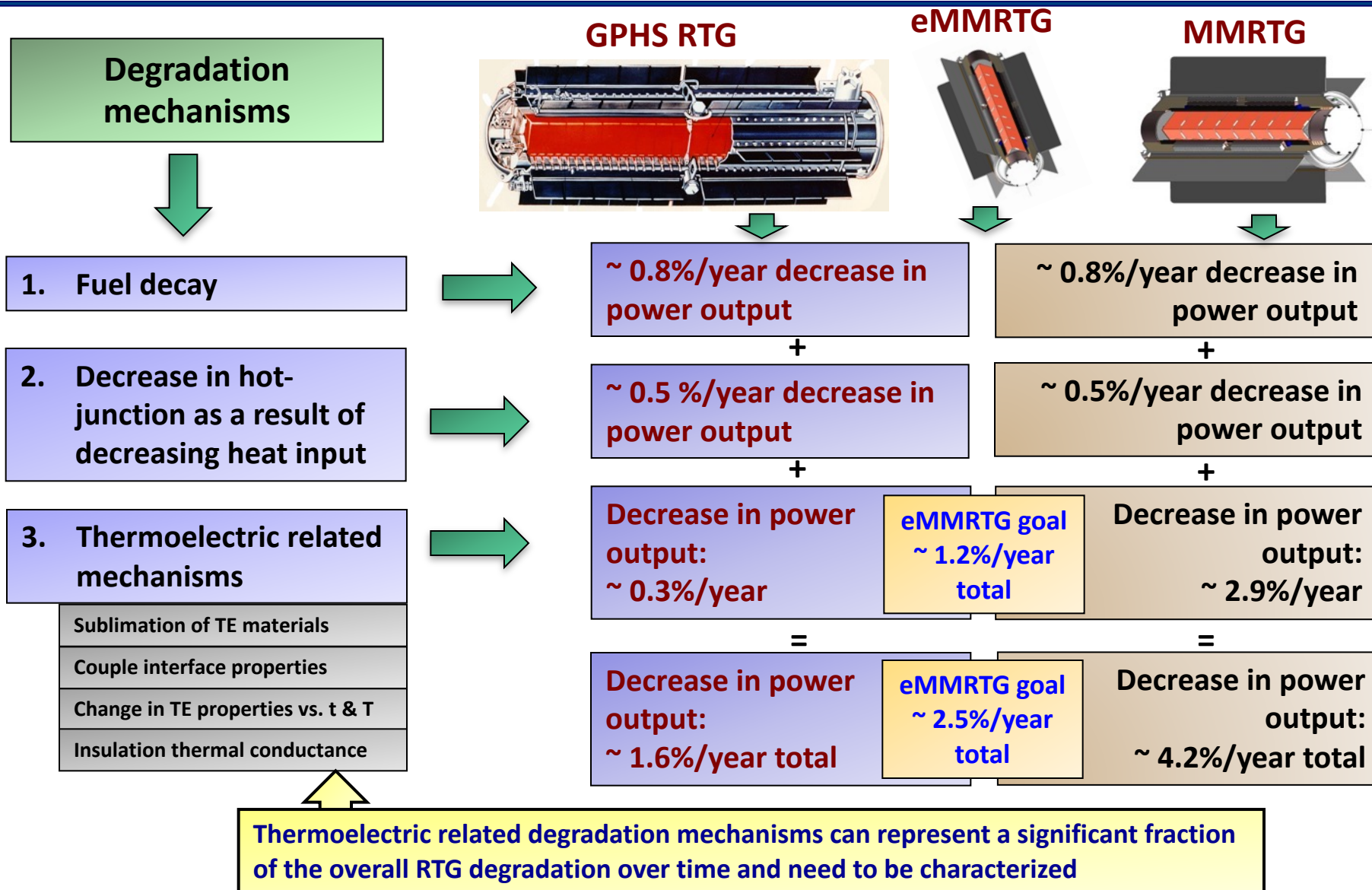
MMLT Couple Testing - P leg Internal resistance



- P-legs less stable over time than n-legs
- 550 and 575° C show better performance than 600° C
- Nominal Thj operating temperature is about 550C



What controls RTGs Lifetime Performance?





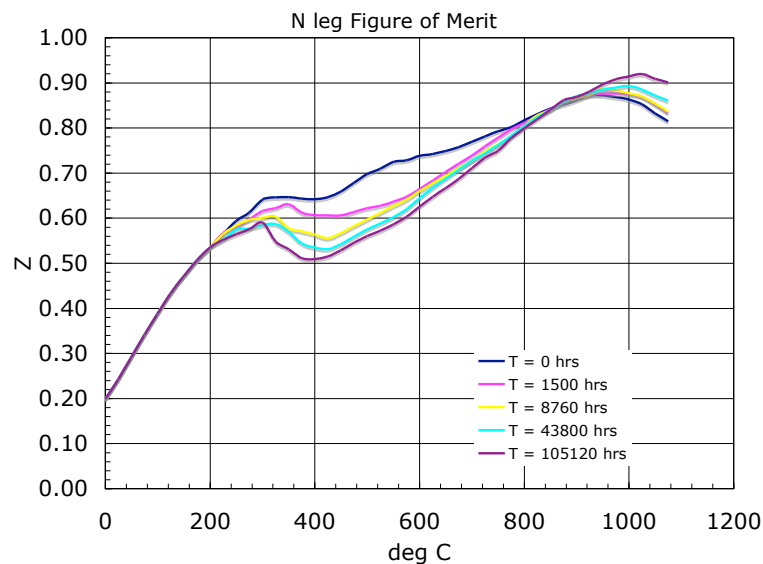
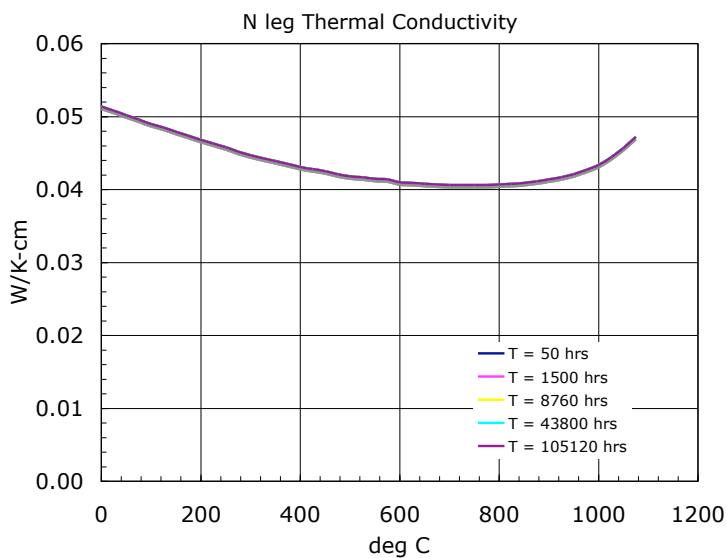
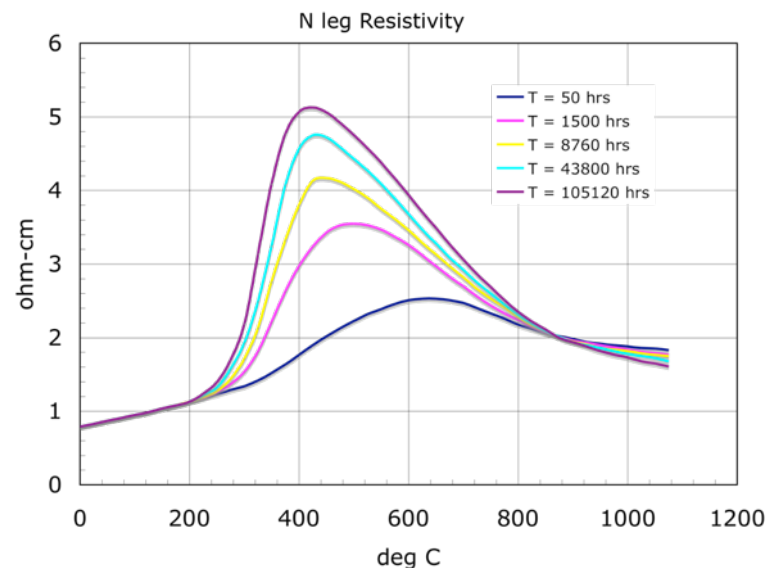
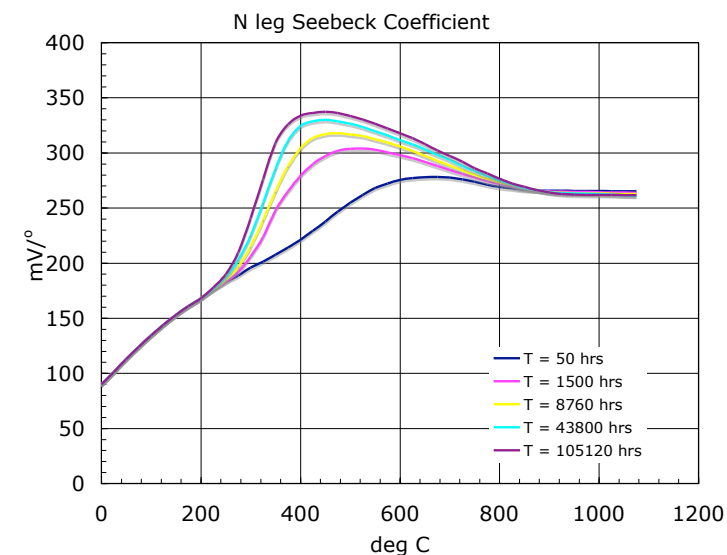
Impact of key TE-related degradation mechanisms on RTG performance

Degradation mechanism	Key potential impact(s)	Impact(s) on generator performance
Sublimation of TE materials	<ul style="list-style-type: none">• Increase in electrical resistance• Electrical and thermal shorts• Promote the degradation of couple interfaces at the hot-junctions• Potentially impact all other mechanisms	<ul style="list-style-type: none">• Reduced power• Electrical isolation
Increase in electrical & thermal contact resistances at the couple interfaces	<ul style="list-style-type: none">• Increase in electrical resistance• Lower temperature gradient across TE elements	<ul style="list-style-type: none">• Reduced power
Change in thermoelectric properties (Seebeck, electrical resistivity, and thermal conductivity) vs. time and temperature	<ul style="list-style-type: none">• Can reduce thermoelectric efficiency if lower ZT• Lower temperature gradient across TE elements if increased thermal conductivity	<ul style="list-style-type: none">• Reduced power
Increase in thermal insulation conductance	<ul style="list-style-type: none">• Increased heat losses• Reduced heat flux through the thermoelectric couples	<ul style="list-style-type: none">• Reduced power• Thermal management

Each TE-related degradation mechanism can have a significant impact on overall RTG degradation over time and must be quantified

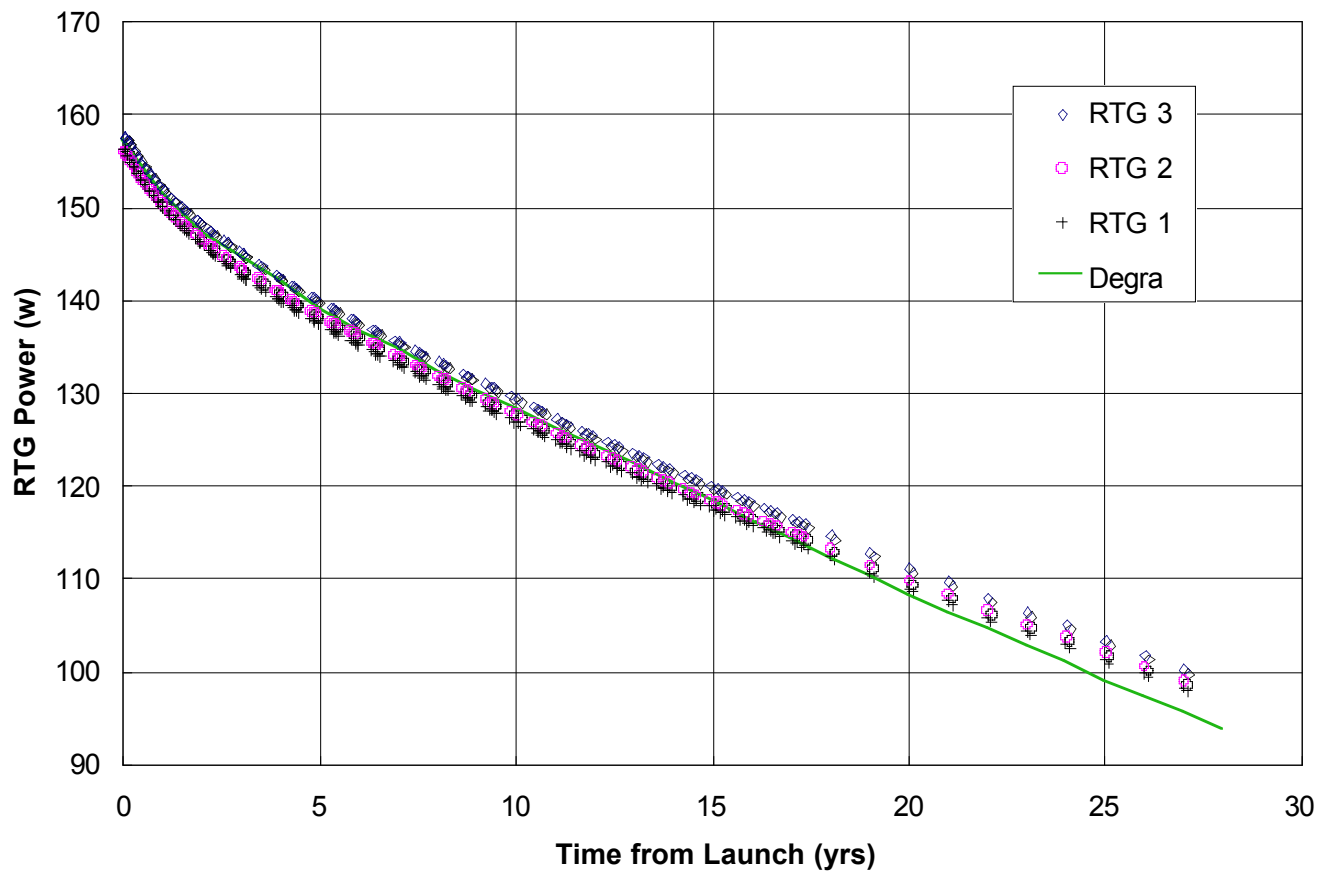


N-SiGe Thermoelectric Property Life Data

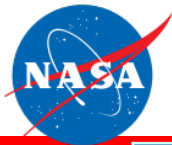




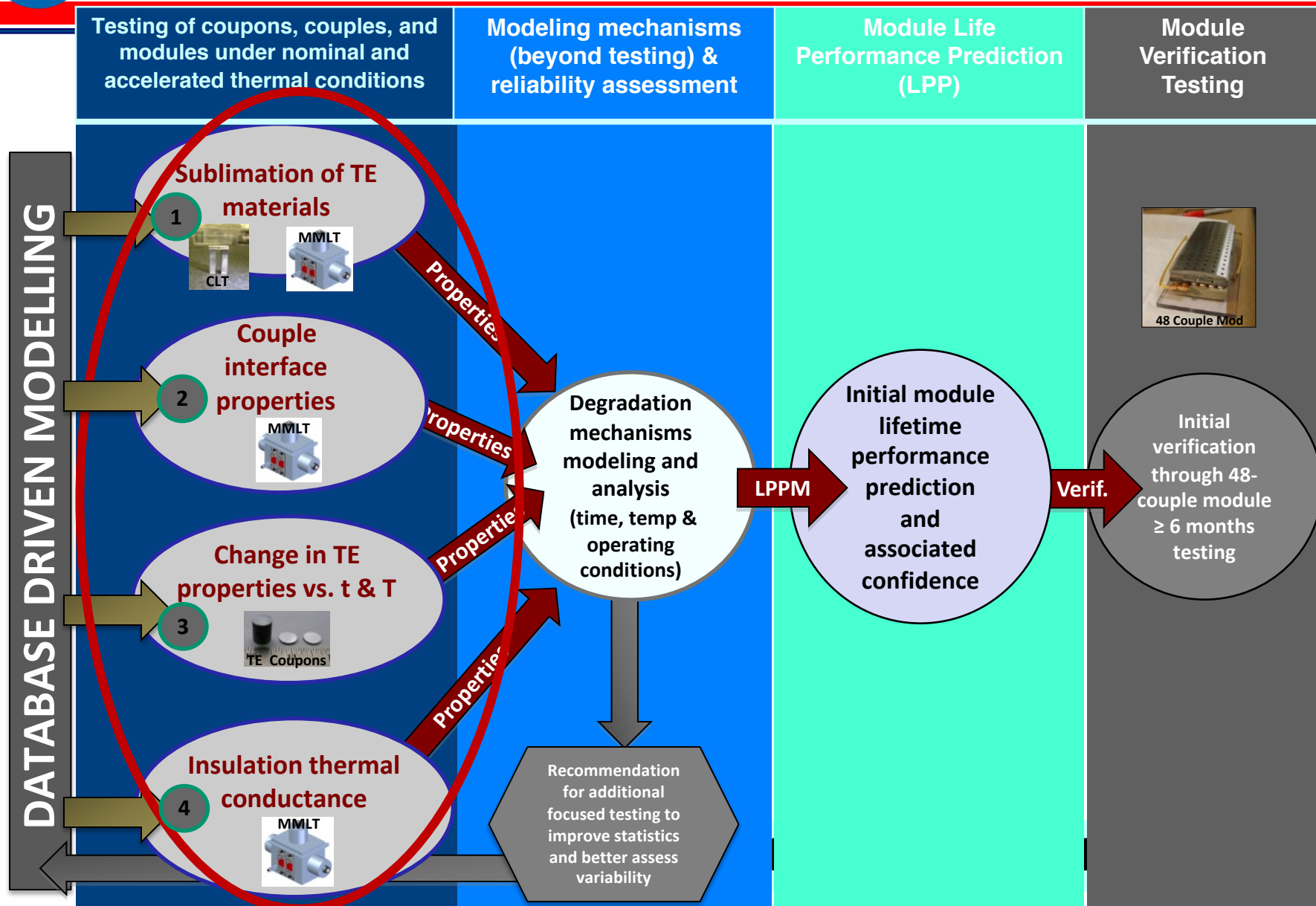
Voyager MHW RTG Performance



MHW-RTG's provided power to Voyager I & II for over ≥ 30 years reliably



eMMRTG Prediction Approach Lifetime Performance

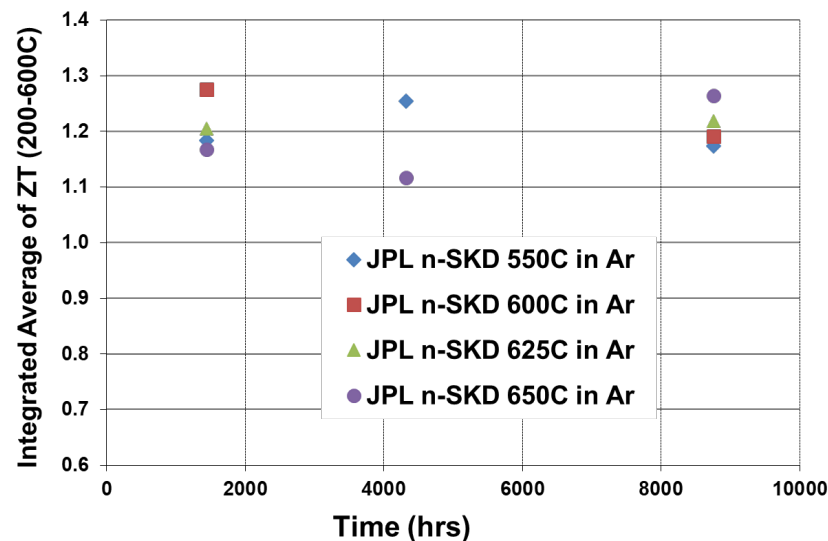
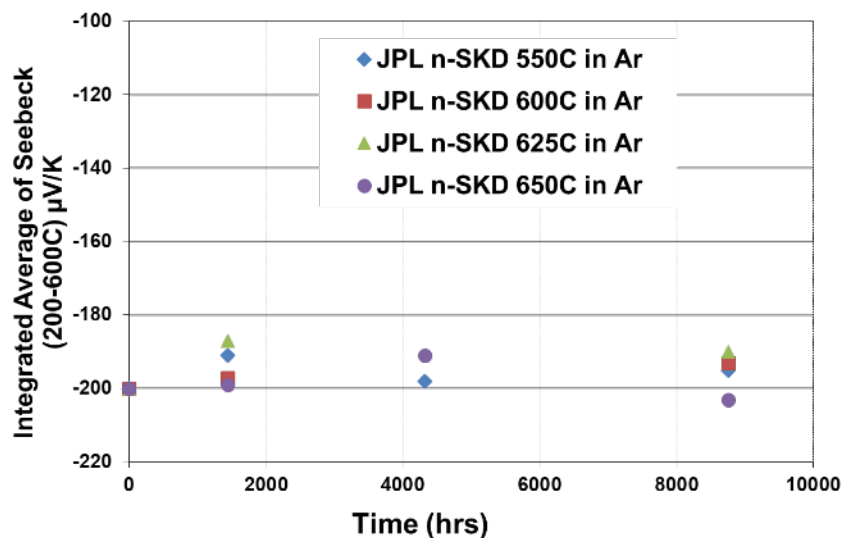
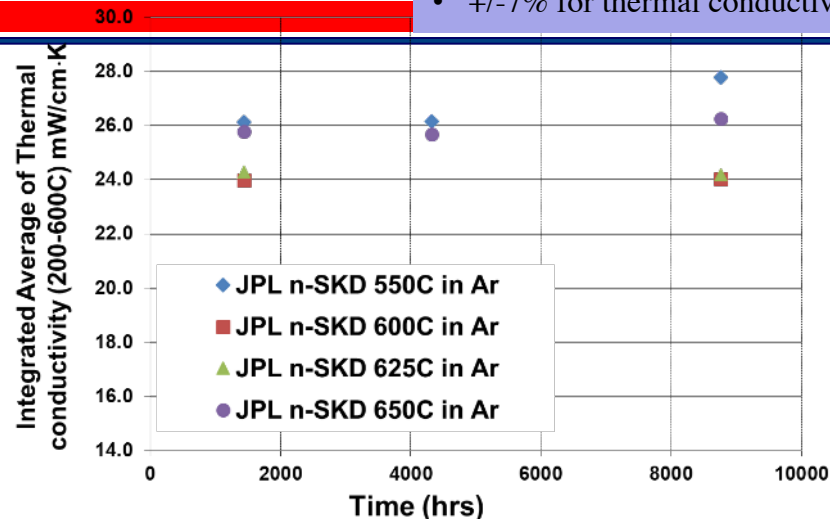
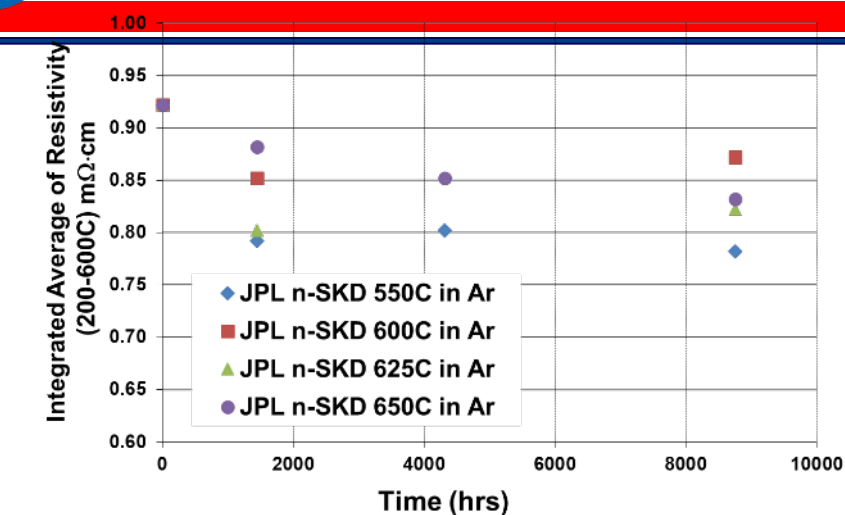




n-SKD TE properties life testing in Ar

Measurement uncertainty:

- $\pm 5\%$ for Seebeck
- $\pm 2\%$ for resistivity
- $\pm 7\%$ for thermal conductivity



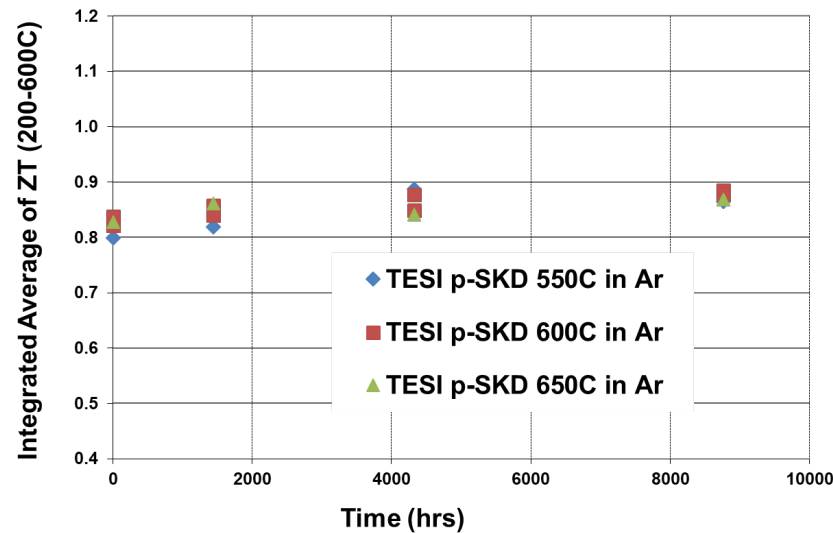
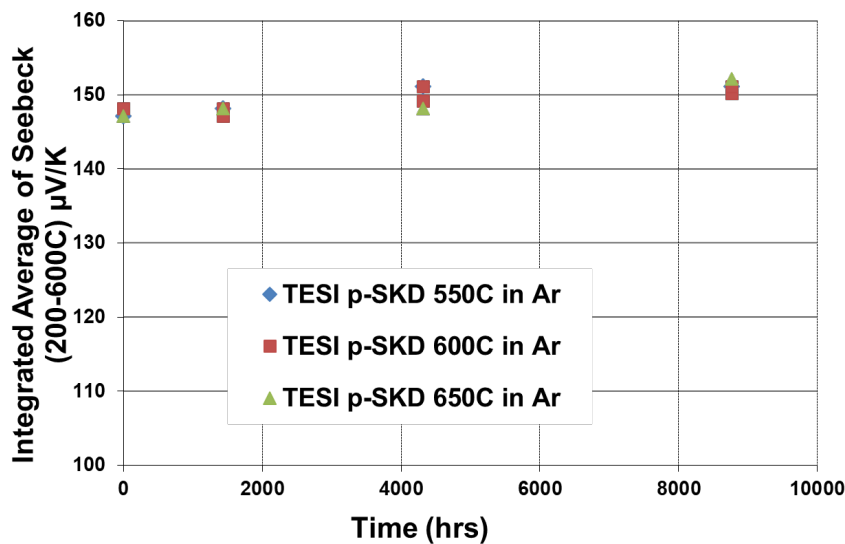
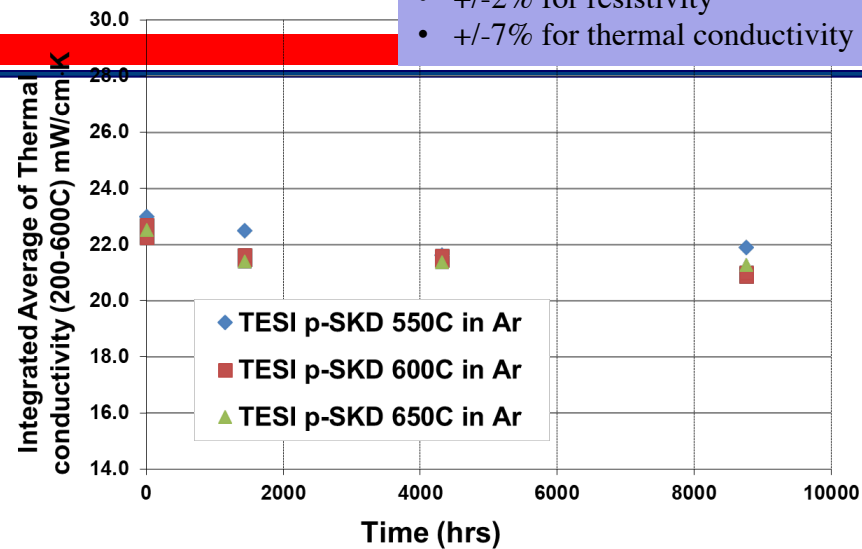
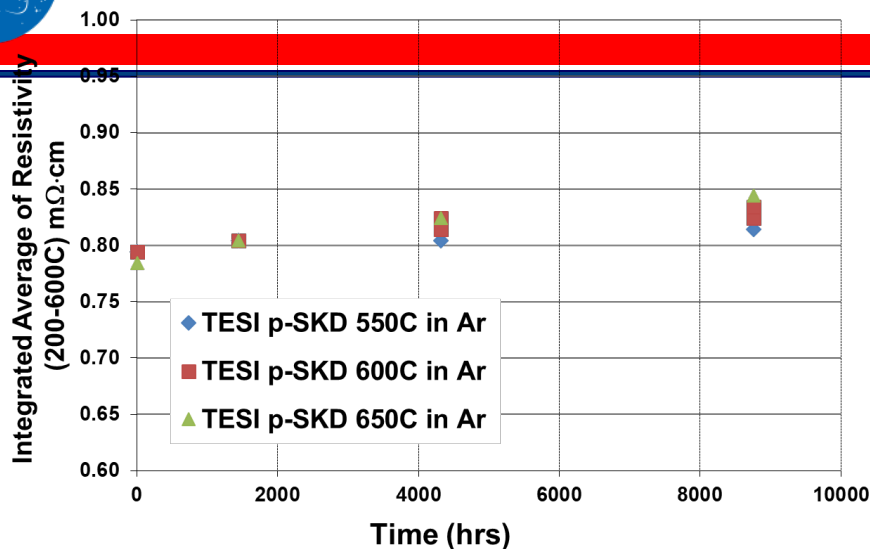
TE properties of n-SKD show no significant trend or change over time



p-SKD TE properties life testing in Ar

Measurement uncertainty:

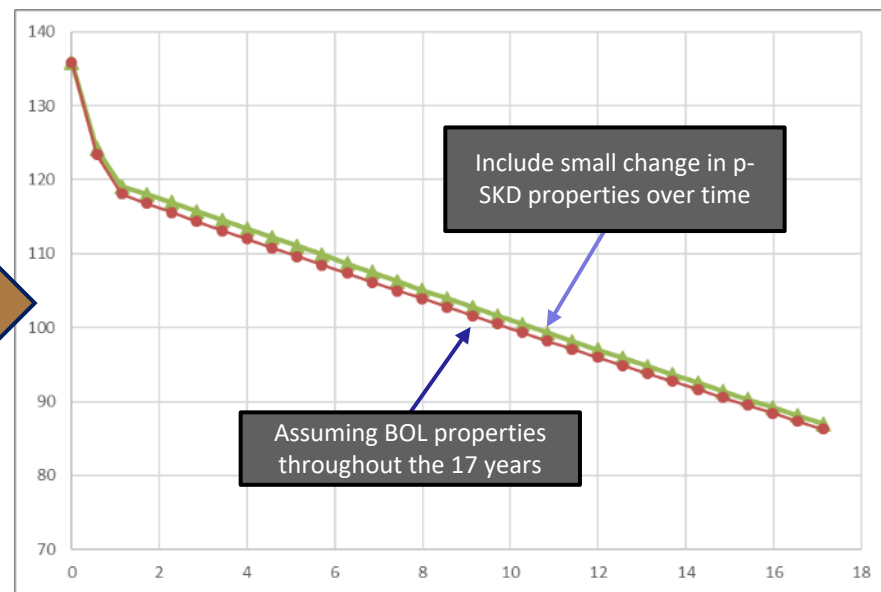
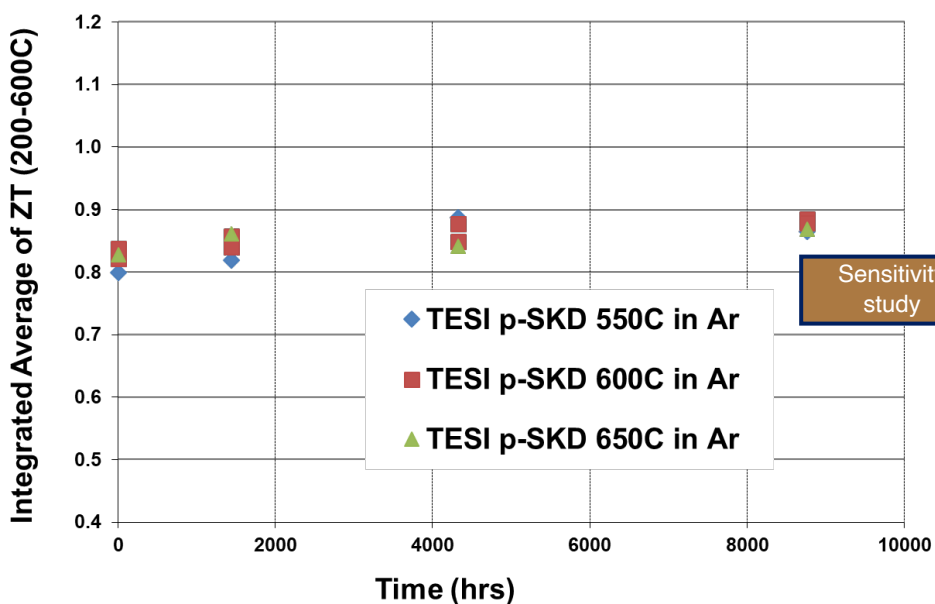
- $\pm 5\%$ for Seebeck
- $\pm 2\%$ for resistivity
- $\pm 7\%$ for thermal conductivity



SKD TE properties of TESI p-SKD show a slight change, increase in ZT, over time



p-SKD TE properties life testing in Ar



- Including the change in p-SKD properties over time increases the EODL power by less than 0.5 W
- Small impact compare to other contributions including couple interface degradation



TE Properties – In-Gradient Life Testing

The couple was tested at $T_H=600^\circ\text{C}$ and $T_C=200^\circ\text{C}$ for 6,360 hours under continuous electrical load $\sim 1.6\text{ A}$

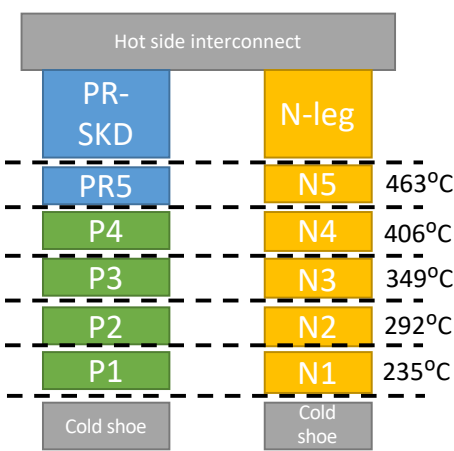
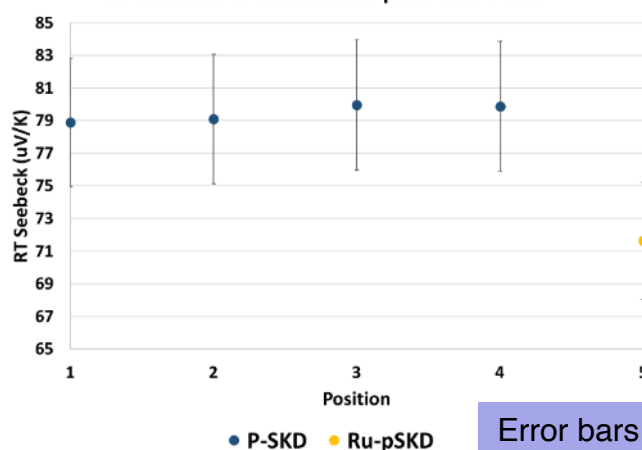
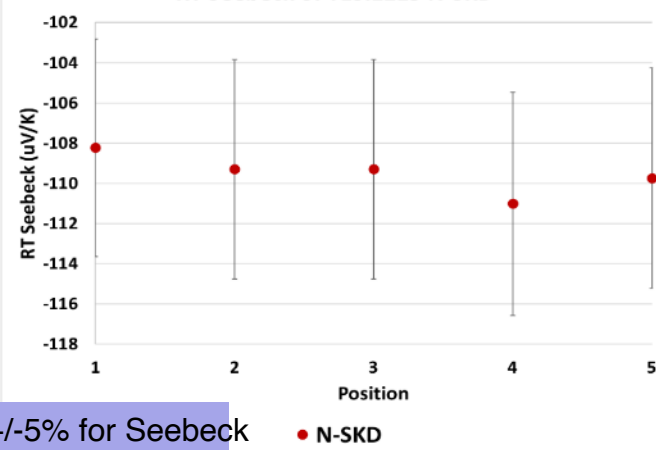


Diagram showing approximate locations and temperatures of sections diced from the SKD legs of couple 1215

RT Seebeck of TESI1215 Ru-pSKD and P-SKD

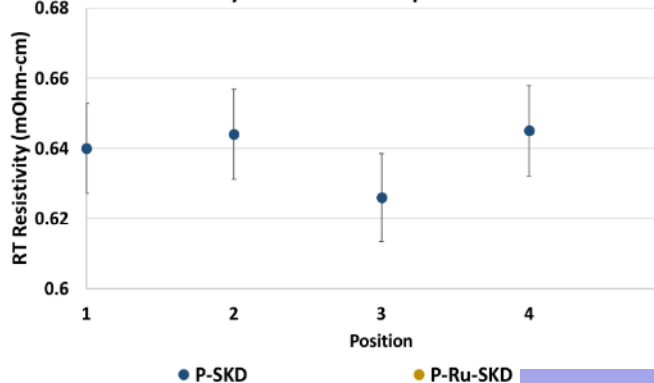


RT Seebeck of TESI1215 N-SKD

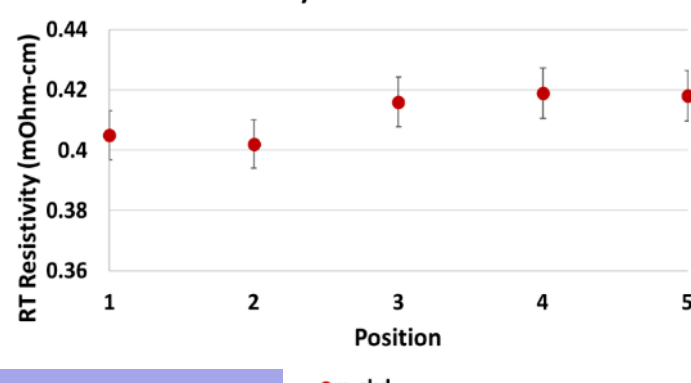


Error bars: +/-5% for Seebeck

RT Resistivity of TESI1215 Ru-pSKD and P-SKD



RT Resistivity of TESI1215 N-SKD



Error bars: +/-2% for resistivity

- Slight changes observed after testing are consistent with isothermal TE property life test results
- No evidence of electromigration or chemically driven TE properties changes



Radiation effects on TE properties

- **Background**

- Potential impact of radiation on TE materials

- TE materials are potentially susceptible to displacement damage from radiation
 - In TE materials, lattice thermal conductivity and other properties may change due to radiation induced displacement damage

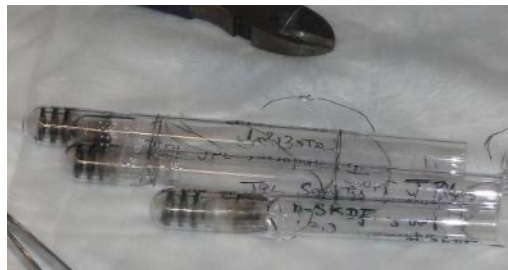
- Source of radiation

- Neutrons from spontaneous fission in undesired plutonium isotopes Pu-236, 240 and 242 in Pu-238 heat source could cause displacement damage
 - Energetic electrons and protons in Europa orbit's natural radiation environment could also cause displacement damage

- **Radiation testing conducted to evaluate potential impact of exposure of SKD materials to radiation**

- **Test conditions**

- Need to include neutrons generated from Pu-238 heat source in the RTG and the 1MeV neutron equivalent fluence for the energetic charged particles in the Europa orbit
 - When these two fluences are added together, and a radiation design factor or radiation design margin of 2 is applied, the total fast neutron fluence is estimated at $2.4 \times 10^{13} \text{ n/cm}^2$
 - The irradiation time inside the OSU-RR at 50kW power was 48.64 minutes to achieve the targeted fast neutron fluence of $2.4 \times 10^{13} \text{ n/cm}^2$
 - Testing was conducted near room temperature



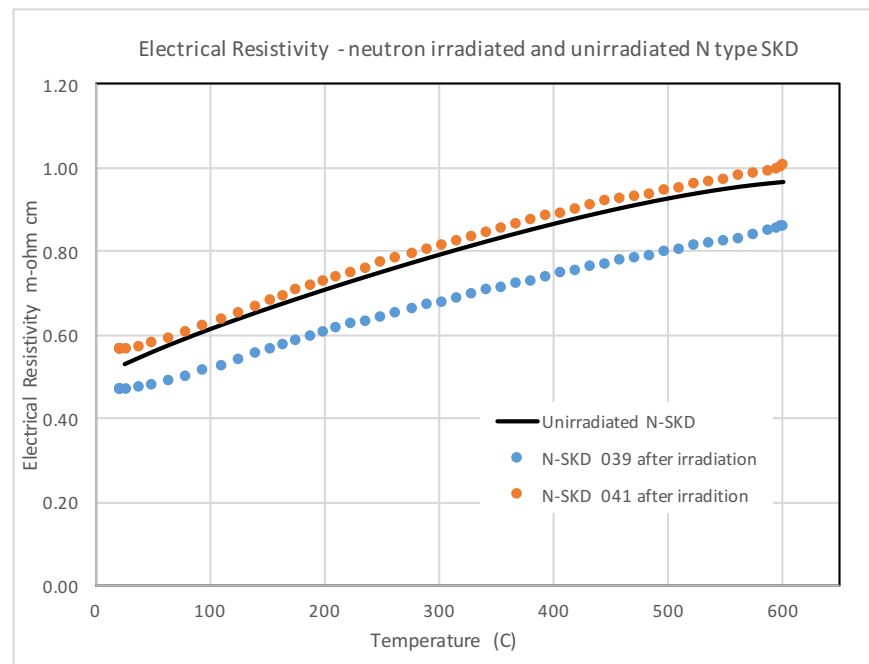
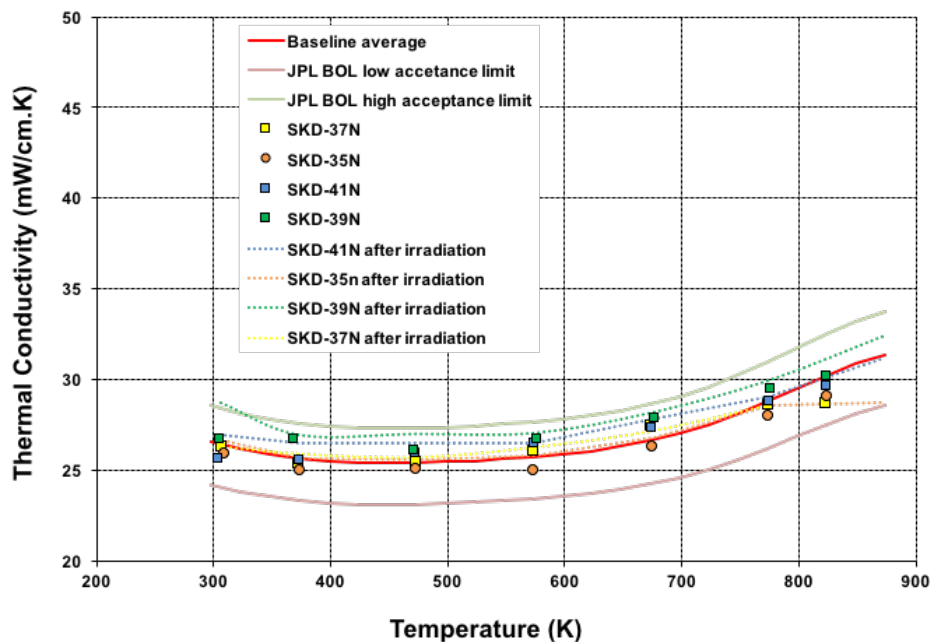
SKD coupons sealed in quartz ampoules for irradiation testing



Photograph showing the Auxiliary Irradiation Column (AIC) inside the research reactor at the Ohio State University



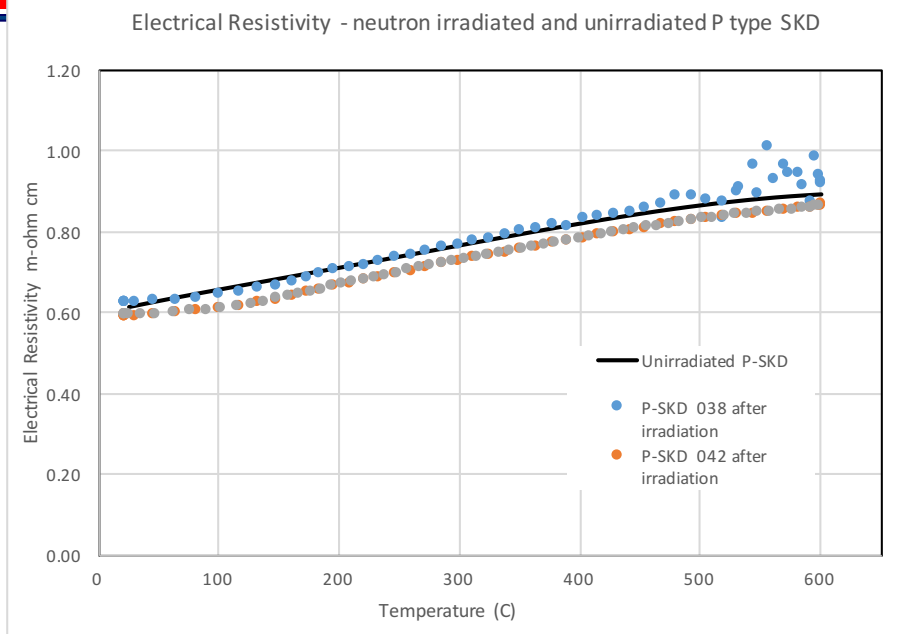
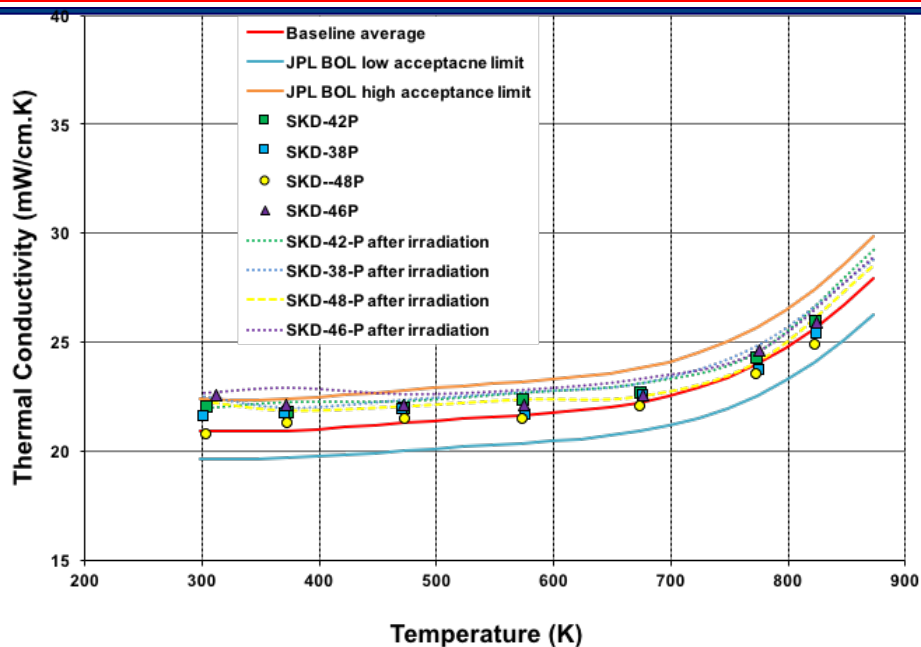
SKD thermal conductivity after irradiation – n-type



Variations between BOL and post-irradiation are within typical measurement uncertainty



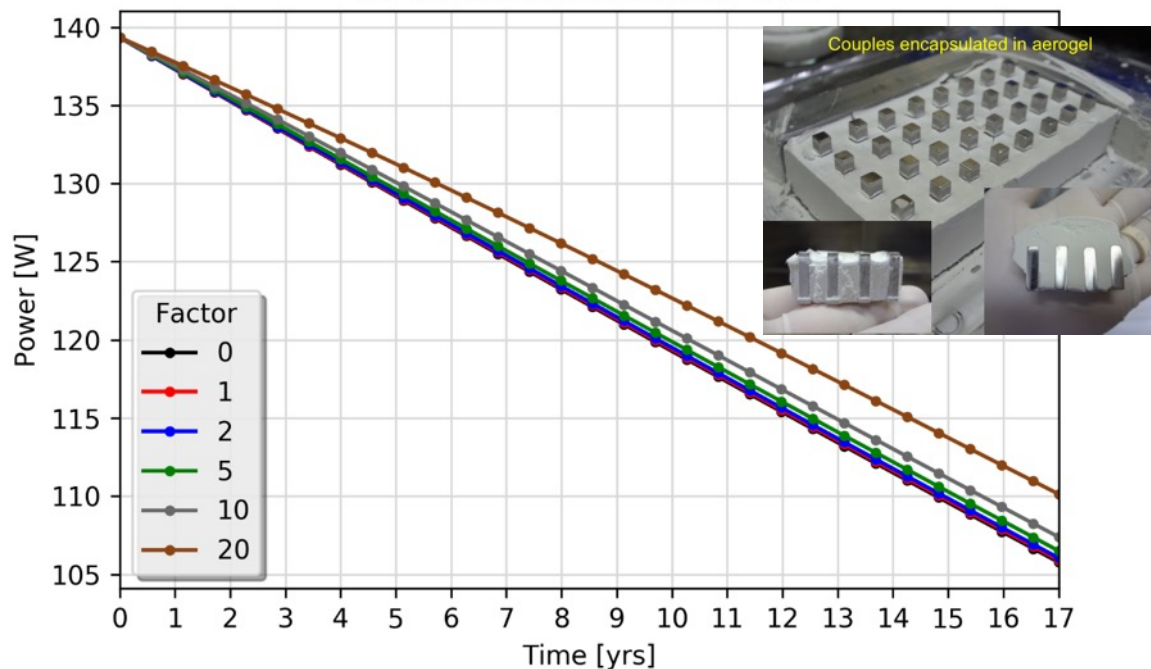
SKD thermal conductivity after irradiation – p-type



Variations between BOL and post-irradiation are within typical measurement uncertainty

Sublimation Rate Testing Status

Power vs Time for Different Multiplicative Factors on Baseline Sublimation Rate



- Factor “0” corresponds to a no sublimation case and Factor “1” corresponds to the sublimation rate established to date for n- and p-SKD materials
- Sublimation rates were also artificially increased up to 20 times to conduct a sensitivity study
- Current estimated sublimation rates are low enough to have little effect on RTG performance



Acknowledgements

- This work is funded by NASA's Radioisotope Power System program managed by NASA Glenn Research Center
- K. Yu, K. Lee, K. Smith, M. Aranda, C. Everline, C. Lee – eMMRTG project